

IMAGE READING IMAGING OPTICAL SYSTEM AND  
IMAGE READING APPARATUS USING THE SAME

BACKGROUND OF THE INVENTION

5 Field of the Invention

This invention relates to an original reading  
imaging optical system and an image reading apparatus  
using the same, and particularly is suitable for  
reading a monochromatic image or a color image using  
10 the line sensor of an image scanner, a digital copier,  
a facsimile apparatus or the like using a compact  
imaging optical element in which various aberrations  
are well-balancedly corrected and which has high  
resolving power.

15 Related Background Art

As an image reading apparatus (image scanner)  
for reading image information on the surface of an  
original, a flat bed type image scanner is proposed,  
for example, in Japanese Patent Application Laid-Open  
20 No. 3-113961.

The flat bed type image scanner is such that an  
imaging lens and a line sensor are fixed and only a  
reflecting mirror is moved to thereby slit-expose and  
scan the surface of an original and read image  
25 information thereon.

In recent years, in order to achieve the  
simplification of the structure of the apparatus, it

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has often become the case that an integral carriage type scanning system in which a mirror, an imaging lens, a line sensor, etc. are made integral with one another to thereby scan the surface of an original is  
5 adopted.

Fig. 32 of the accompanying drawings is a schematic view of the essential portions of an image reading apparatus of the integral carriage type scanning system according to the prior art. In Fig.  
10 32, a beam emitted from an illuminating light source 1 illuminates an original 8 directly placed on an original supporting table 2, and the reflected beam from the original 8 has its optical path bent in the interior of a carriage 6 through first, second and  
15 third reflecting mirrors 3a, 3b and 3c in the named order, and is imaged on the surface of a line sensor 5 by an imaging lens (imaging optical system) 4. The carriage 6 is moved in the direction of arrow A (sub scanning direction) indicated in Fig. 32 by a sub  
20 scanning motor 7 to thereby read the image information of the original 8. The line sensor 5 in Fig. 32 is of a construction in which a plurality of light receiving elements are arranged in one-dimensional direction (main scanning direction).

25 Fig. 33 of the accompanying drawings is an illustration of the basic construction of the image reading optical system of Fig. 32.

In Fig. 33, the reference numeral 4 designates an imaging optical system, the reference characters 5R, 5G and 5B denote line sensors for the respective colors R(red), G(green) and B(blue) of the line sensor 5, and the reference characters 8R, 8G and 8B designate reading ranges on the surface of the original corresponding to the line sensors 5R, 5G and 5B. In the image reading apparatus shown in Fig. 32, the surface of the stationary original is scanned by the carriage 6, but the carriage scanning is equivalent to the line sensor 5 and the imaging lens being stationary and the surface of the original 8 being moved, as shown in Fig. 33. By the surface of the original being scanned, the same location can be read in different colors at a certain time interval. When in the aforescribed construction, the imaging lens 4 comprises an ordinary refracting system, on-axis chromatic aberration and chromatic aberration of magnification occur and therefore, relative to the reference line sensor 5G, defocus or positional deviation occurs to line images formed on the line sensors 5B and 5R. Accordingly, when images of the respective colors are superimposed and reproduced, the images become images in which color oozing and misregister are conspicuous. That is, when such performance as high aperture or high resolution is required, the requirement cannot be coped with.

On the other hand, recently, in a non-coaxial optical system as well, it has become apparent that the concept of a reference axis is introduced and a constituent surface is made into an asymmetrical aspherical surface, whereby an optical system in which aberrations have been sufficiently corrected can be constructed. The example, a designing method for it is shown in Japanese Patent Application Laid-Open No. 9-5650, and examples of the design thereof are shown in Japanese Patent Application Laid-Open Nos. 8-292371 and 8-292372.

Such a non-coaxial optical system is called an off-axial optical system (which is an optical system defined as an optical system containing a curved surface (an off-axial curved surface) in which, when considering a reference axis along a ray of light passing through the center of an image and the center of a pupil, a surface normal at the point of intersection of a constituent surface with the reference axis is not on the reference axis, and in this case, the reference axis is of a bent shape). This off-axial optical system is such that the constituent surface thereof generally is non-coaxial and eclipse does not occur even on the reflecting surface thereof and therefore, an optical system using a reflecting surface is easy to construct. It also has the features that the drawing around of an

optical path can be effected relatively freely and that an integral type optical system is easy to make by the technique of integrally molding a constituent surface.

5           On the other hand, high resolution and a high speed are required of an original reading system such as a digital copier and therefore, such system has not yet come to be constituted by an integral type optical system. An imaging lens required in the  
10   reading system needs to be bright and high in resolution and therefore, to secure optical performance, it is difficult to make the angle of field great. If the angle of field is narrow, the optical path length will become long as the result.

15           On the other hand, when the reading of a color image is to be effected, as the resolution becomes higher, the imaging position difference for each color by chromatic aberration, and chromatic aberration such as color misregister in an image  
20   field adversely affect optical performance.

#### SUMMARY OF THE INVENTION

It is an object of the present invention to provide, in an original reading system such as a  
25   digital copier of which a high speed and high resolution are required, an original reading imaging optical system which can easily realize an integral

carriage type scanning process, and an image reading apparatus using the same.

It is also an object of the present invention to provide, in the reading of a digital color image, an  
5 original reading imaging optical system which is free of chromatic aberration and can easily realize an integral carriage type scanning process, and an image reading apparatus using the same.

Also, when generally an off-axial reflecting  
10 surface is used as an imaging optical element, a reference axis ray is obliquely incident on and reflected by each off-axial reflecting surface so that an imaged beam may not be intercepted and therefore, asymmetrical aberration occurs originally.

It is an object of the present invention to  
15 provide an original reading imaging optical system in which, even if the imaging optical system is constituted by an off-axial reflecting surface, the occurrence of asymmetrical aberration is little and  
20 optical performance is not greatly deteriorated, and an image reading apparatus using the same.

In one aspect of the invention, there is provided an image reading imaging optical system for  
imaging image information on a line sensor and  
25 reading the image information, characterized by an imaging optical element including a plurality of off-axial reflecting surfaces differing in the direction

of incidence and the direction of emergence of a reference axis ray from one another and having curvatures.

In further aspect of the foregoing image reading  
5 imaging optical system, said imaging optical element has the function of changing the direction of emergence to a direction substantially perpendicular or opposite to the direction of incidence of the reference axis ray.

10 In further aspect of the foregoing image reading imaging optical system, said imaging optical element comprises a plurality of off-axial reflecting surfaces including at least one set of reflecting surfaces intersecting with each other, and has a stop  
15 between the off-axial reflecting surfaces intersecting with each other.

In another aspect of the invention, there is provided an image reading apparatus which includes an original supporting table on which an original is  
20 placed, an imaging optical element and a line sensor, and in which image information on the surface of the original is imaged on the line sensor by the imaging optical element, and the image information is read by said line sensor, and said imaging optical element  
25 has a plurality of off-axial reflecting surfaces differing in the direction of incidence and the direction of emergence of a reference axis ray from





element and the direction of the reference axis ray emerging from said imaging optical element are substantially opposite directions.

In further aspect of the foregoing image reading  
5 imaging optical system, said image information is not intermediately imaged in said imaging optical element, but is directly formed on the line sensor.

In further aspect of the foregoing image reading  
10 imaging optical system, said imaging optical element has a stop near substantially the center of the optical path between the light incidence surface and the light exit surface thereof.

In further aspect of the foregoing image reading  
15 imaging optical system, said stop is formed by the effective surface of an off-axial reflecting surface located near substantially the center of the optical path between the light incidence surface and the light exit surface of said imaging optical element.

In further aspect of the foregoing image reading  
20 imaging optical system, an internal medium constituting said imaging optical element is air.

In further aspect of the foregoing image reading  
imaging optical system, an internal medium  
constituting said imaging optical element is  
25 optically transparent glass or plastic.

In further aspect of the foregoing image reading  
imaging optical system, when the off-axial reflecting

surface for counter-clockwisely deflecting the  
reference axis ray is defined as a plus deflecting  
surface, and the off-axial reflecting surface for  
clockwisely deflecting the reference axis ray is  
5 defined as a minus deflecting surface, said imaging  
optical element has at least one set of constructions  
in which the plus deflecting surface is continuous or  
at least one set of constructions in which the minus  
deflecting surface is continuous.

10 In further aspect of the foregoing image reading  
imaging optical system, when the off-axial reflecting  
surface for counter-clockwisely deflecting the  
reference axis ray is defined as a plus deflecting  
surface, and the off-axial reflecting surface for  
15 clockwisely deflecting the reference axis ray is  
defined as a minus deflecting surface, said imaging  
optical element has at least one set of constructions  
in which the plus deflecting surface is continuous  
and at least one set of constructions in which the  
20 minus deflecting surface is continuous.

In further aspect of the foregoing image reading  
imaging optical system, said imaging optical element  
is comprised of six off-axial reflecting surfaces,  
and when the off-axial reflecting surface for  
25 counter-clockwisely deflecting the reference axis ray  
is defined as a plus deflecting surface, and the off-  
axial reflecting surface for clockwisely deflecting

5 surface most adjacent to the exit side is disposed on  
the original side on the incidence reference axis  
relative to the off-axial reflecting surface most  
adjacent to the incidence side.

10 imaging optical system, said plus deflecting surfaces  
and said minus deflecting surfaces are disposed so as  
to be opposite deflecting surfaces relative to a stop.

15 surface of said imaging optical element which is most  
adjacent to the incidence side is designed to have  
the converging action.

20 imaging optical element has a characteristic of  
cutting infrared light.

25 original in parallel to a reflecting mirror.

In further aspect of the foregoing image reading imaging optical system, when the effective beam width

in a direction perpendicular to the line direction of  
the line sensor on the exit surface of said imaging  
optical element is defined as  $\Phi_s$ , and the effective  
beam width in the line direction of the line sensor  
5 is defined as  $\Phi_m$ , the condition that

$$\Phi_s < \Phi_m$$

is satisfied.

In another aspect of the invention, there is  
provided an image reading apparatus which includes an  
10 original supporting table on which an original is  
placed, an imaging optical element and a line sensor,  
and in which image information on the surface of the  
original is imaged on the line sensor by the imaging  
optical element and the image information is read by  
15 said line sensor, and the image reading apparatus  
further includes a reflecting mirror and an imaging  
optical element for reflecting a reference axis ray a  
plurality of times, and said imaging optical element  
has the function of changing the direction of  
20 emergence to a direction substantially perpendicular  
or opposite to the direction of incidence of the  
reference axis ray.

In further aspect of the foregoing image reading  
imaging optical system, said imaging optical element  
25 has a plurality of off-axial reflecting surfaces  
differing in the direction of incidence and the  
direction of emergence of the reference axis ray from

one another and having curvatures.

In further aspect of the foregoing image reading imaging optical system, the bending direction of the reference axis ray on each off-axial reflecting surface is in a cross section perpendicular to the line direction of said line sensor.

In further aspect of the foregoing image reading imaging optical system, at least two reflecting mirrors are provided.

10 In further aspect of the foregoing image reading imaging optical system, said imaging optical element is disposed on the side opposite to the surface of said original with respect to said reflecting mirror.

15 In further aspect of the foregoing image reading imaging optical system, said imaging optical element is disposed in a housing along the surface of said original in parallel to said reflecting mirror.

20 In still another aspect of the invention, there is provided an image reading apparatus which includes an original supporting table on which an original is placed, an imaging optical element and a line sensor, and in which image information on the surface of the original is imaged on the line sensor and the image information is read by said line sensor, and said  
25 imaging optical element includes a plurality of off-axial reflecting surfaces including at least one set of reflecting surfaces intersecting with each other,

and has a stop between the off-axial reflecting surfaces intersecting with each other.

In further aspect of the foregoing image reading imaging optical system, the bending direction of a  
5 reference axis ray on each off-axial reflecting surface of said imaging optical element is in a cross section perpendicular to the line direction of said line sensor.

In further aspect of the foregoing image reading  
10 imaging optical system, the stop in said imaging optical element is disposed near substantially the center of the optical path between the light incidence surface and the light exit surface of the imaging optical element.

15 In further aspect of the foregoing image reading imaging optical system, said stop differs in the aperture width thereof in a cross section perpendicular to the line direction of the sensor line and the aperture width in a direction parallel  
20 to the line direction.

In further aspect of the foregoing image reading imaging optical system, said stop is constructed integrally with the off-axial reflecting surfaces proximate thereto.

25 In further aspect of the foregoing image reading imaging optical system, said image information is a color image.

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Fig. 9 shows the aberrations of Embodiment 3 of

Fig. 10 is a cross-sectional view of the essential portions of Embodiment 4 of the image reading imaging optical system of the present invention.

Fig. 12 is a cross-sectional view of the essential portions of Embodiment 6 of the image reading imaging optical system of the present invention.

Fig. 14 is a cross-sectional view of the  
20 essential portions of Embodiment 8 of the image  
reading imaging optical system of the present  
invention.

Fig. 16 is a schematic view of the essential portions of Embodiment 9 of the image reading





portions of Embodiment 14 of the image reading  
imaging optical system of the present invention.

Fig. 26 is a schematic view of the essential  
portions of Embodiment 14 of the image reading  
5 apparatus of the present invention.

Fig. 27 is a schematic view of the essential  
portions of Embodiment 15 of the image reading  
imaging optical system of the present invention.

Fig. 28 is a schematic view of the essential  
10 portions of Embodiment 15 of the image reading  
apparatus of the present invention.

Fig. 29 is a schematic view of the essential  
portions of Embodiment 16 of the image reading  
imaging optical system of the present invention.

Fig. 30 is a schematic view of the essential  
15 portions of Embodiment 16 of the image reading  
apparatus of the present invention.

Fig. 31 illustrates the definition of the off-  
axial optical system of an imaging optical element  
20 according to the present invention.

Fig. 32 shows an example of the arrangement of  
an integral carriage type scanning optical system  
according to the prior art.

Fig. 33 is a schematic view of essential  
25 portions illustrating a color image reading apparatus  
according to the prior art.

Fig. 34 is a cross-sectional view of the

essential portions of Embodiment 17 of the image reading imaging optical system of the present invention.

Fig. 35 shows the aberrations of Embodiment 17 of the image reading imaging optical system of the present invention.

Fig. 36 is a schematic view of the essential portions of Embodiment 17 of the image reading apparatus of the present invention.

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#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Figs. 1A to 1C are illustrations of Embodiment 1 of an image reading imaging optical system used in the image reading apparatus of the present invention.

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Fig. 1A is a sub scanning cross-sectional view, Fig. 1B is a main scanning cross-sectional view, and Fig. 1C is a perspective view of essential portions.

Fig. 2 is a schematic view of essential portions when the image reading imaging optical system of Figs. 1A to 1C is applied to the image reading apparatus of an integral type scanning optical system.

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The details of the embodiments of the present invention will hereinafter be described with reference to the drawings.

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The imaging optical system (image reading imaging optical system) of the image reading apparatus of the present invention is designed such

that the optical path length is short and basically the occurrence of chromatic aberration is little, by the utilization of an imaging optical element chiefly including a plurality of off-axial reflecting surfaces having curvatures. In some cases, the image reading imaging optical system also has a lens, a mirror, etc. In Figs. 1A to 1C, an imaging optical element 4a has five off-axial reflecting surfaces (R3 to R7) of which the internal medium is optical resin and in which the direction of the incident ray LP1 of a reference axis ray and the direction of the emergent ray LP0 thereof differ from each other and which have curvatures, and has the function of causing an image on an original surface 8 to be imaged on a line sensor 5. Each off-axial reflecting surface adopts a construction for bending an optical path in a cross section in a direction (Y direction) perpendicular to a line in a direction (X direction) in which the sensors of the line sensor 5 are arranged, i.e., a sub scanning cross section (YZ cross section).

Also, the off-axial reflecting surface for deflecting the reference axis ray in a counter-clockwise direction is defined as a plus deflecting surface, and the off-axial reflecting surface for deflecting the reference axis ray in a clockwise direction is defined as a minus deflecting surface.

At this time, the imaging optical element 4a of Figs. 1A and 1B is of an arrangement in which in succession from the original surface 8 side, the surface R3 is a plus deflecting surface, the surface R4 is a plus  
5 deflecting surface, the surface R5 is a minus deflecting surface, the surface R6 is a minus deflecting surface and the surface R7 is a plus deflecting surface.

As the result, the direction of the reference  
10 axis ray LP0 emerging from an exit surface R8 becomes substantially perpendicular to the direction of the incident reference axis ray LPI. The plus deflecting surfaces continue the arrangement of the deflecting surfaces, and thereafter the minus deflecting  
15 surfaces continue it, whereby the optical path travels in a direction substantially orthogonal to the incident ray and therefore, the imaging optical element 4a can assume a spatially efficient disposition.

20 Fig. 1A shows an optical path in a cross section perpendicular to the line direction (X direction) of the line sensor 5, i.e., a sub scanning cross section, and Fig. 1B shows an optical path in a cross section parallel to the line direction of the line sensor 5,  
25 i.e., a main scanning cross section (XZ cross section). Fig. 1C shows a perspective view of the optical paths of the imaging optical element 4a.

As can be seen from Figs. 1A and 1B, in the main scanning cross section, the beam width widens away from a stop surface SP, but in the sub scanning cross section, the beam width scarcely varies irrespective of each surface. That is, when the effective beam width in a direction perpendicular to the line direction (X direction) of the line sensor 5 on the exit surface R8 of the imaging optical element 4a, i.e., the sub scanning direction (Y direction) is defined as  $\Phi_s$ , and the effective beam width in the line direction of the line sensor 5, i.e., the main scanning direction (X direction) is defined as  $\Phi_m$ , the following condition is satisfied:

$$\Phi_s < \Phi_m$$

Accordingly, to construct the image reading apparatus compactly, it is preferable to bend the optical path in the sub scanning cross section. By this bending of the optical path, there can be adopted a construction suited for an integral carriage type scanning optical system. In Embodiment 1, the converging power of each off-axial reflecting surface is designed such that positive converging power and negative converging power are alternately arranged so that good imaging performance may be obtained.

In the construction of the reflecting surfaces, to construct them so as not to mutually intercept the

optical path, it is unavoidable to secure the spacing between adjacent surfaces greatly to a certain extent. Accordingly, it is preferable to dispose a surface of a different characteristic near them to thereby

5 correct aberrations. Preferably the arrangement of the converging power for that purpose may be such that positive converging power and negative converging power are alternately arranged.

In Embodiment 1, the image on the original  
10 surface is designed not to be intermediately imaged in the imaging optical element 4a, but to be directly imaged on the line sensor 5 after having emerged from the imaging optical element 4a. Thereby the curvature of each off-axial reflecting surface can be  
15 made gently and therefore it becomes easy to suppress aberrations occurring in each reflecting surface. Because of the construction in which the image on the original surface is not intermediately imaged in the imaging optical element 4a, in the line direction (X  
20 direction) of the line sensor 5, the beam widens as it moves away from the stop SP. In Embodiment 1, the stop SP is set on the off-axial reflecting surface near the center of the optical path of the imaging optical element 4a so that the effective beams on the  
25 incidence surface R2 and exit surface R8 of the imaging optical element 4a may not become large in the main scanning direction. This also contributes

to the compact construction of the imaging optical element 4a.

In addition to the adoption of the above-described construction, the off-axial reflecting surfaces are made into free-form surfaces to thereby secure desired optical performance. Also, in Embodiment 1, the incidence surface R2 and the exit surface R8 are refracting surfaces and this becomes a factor which causes chromatic aberration to occur. So, both surfaces are made into free-form surfaces to thereby suppress the occurrence of chromatic aberration and also effect the correction of the other aberrations than chromatic aberration. In Embodiment 1, the medium between adjacent off-axial reflecting surfaces is formed of optically transparent plastic PMMA. It may also be formed of glass.

Fig. 2 shows an example of an original reading apparatus for reading a color image or a monochromatic image which is constructed by the use of the imaging optical element 4a of Embodiment 1 shown in Figs. 1A to 1C. When the image reading apparatus of the present invention takes up a color image as an object, it uses the sensor shown in Fig. 33.

In Fig. 2, the reference numeral 1 designates a light source, the reference numeral 2 denotes an



original supporting glass table, the reference characters 3a and 3b designate first and second reflecting mirrors, the reference character 4a denotes the imaging optical element, the reference numeral 5 designates the line sensor comprised of a CCD or the like, and the reference numeral 6 denotes a carriage (housing).

An original 8 placed on the original supporting glass table 2 can be imaged on the line sensor 5 by the imaging optical element 4a through the intermediary of the mirrors 3a and 3b and one line of the original 8 can be read. In order to construct the original reading apparatus compactly, the optical path is folded by the first and second reflecting mirrors 3a and 3b. The imaging optical element 4a also contributes to folding the optical path. By using the imaging optical element 4a, the original reading apparatus of the integral carriage type optical system can be comprised of a few optical parts comprising the two mirrors and the imaging optical element.

As compared with the conventional construction of Fig. 32, the optical path is bent substantially at a right angle by only the imaging optical element and this corresponds to the adoption of a construction including a mirror in an imaging optical system, and the image reading apparatus can be made into a simple

construction. This integral carriage type optical system scans the original 8 and the carriage 6 relative to each other in a direction perpendicular to the line direction (X direction) of the line sensor, i.e., the sub scanning direction (Y direction or A direction) to thereby two-dimensionally read the surface of the original 8.

Fig. 3 shows the aberrations about five points (image heights) in the line direction of the line sensor in Embodiment 1. In Fig. 3, X is representative of the height on the surface of the original.

Fig. 4 is a cross-sectional view of the essential portions of Embodiment 2 of the imaging optical element of the present invention.

The imaging optical element 4b of Embodiment 2 is such that the direction of the exit surface R9 relative to the incidence surface R2 for the reference axis ray is the same, and only off-axial reflecting surfaces having curvatures are comprised of six surfaces (R3 to R8). The medium between adjacent reflecting surfaces is air, and is of a hollow construction in which basically chromatic aberration does not occur. By even number of times of reflection, the direction of the incident ray and the direction of the exit ray become substantially the same direction.

The imaging optical element 4b of Fig. 4 is of an arrangement in which, in succession from the original surface 8 side, the surface R3 is a plus deflecting surface, the surface R4 is a minus  
5 deflecting surface, the surface R5 is a minus deflecting surface, the surface R6 is a plus deflecting surface, the surface R7 is a plus deflecting surface, and the surface R8 is a minus deflecting surface.

10 As the result, the direction of the exit reference axis ray is substantially the same direction as the direction of the incident reference axis ray. The arrangement of the deflecting surfaces is made such that a set in which the minus deflecting  
15 surfaces continue and a set in which the plus deflecting surfaces continue are alternately arranged, whereby the optical path travels in a direction substantially parallel to the incident ray and therefore, the imaging optical element 4b can assume  
20 a spatially efficient disposition.

In Embodiment 2, as in Embodiment 1, the image of the original is designed not to be intermediately imaged in the imaging optical element 4b, but to be directly formed on the line sensor 5 so that the  
25 curvature of each off-axial reflecting surface can be constructed gently. Further, the stop SP is disposed near the center of the optical path of the imaging

optical element 4b so that the effective beams on the incidence surface R2 and exit surface R9 of the imaging optical element 4b may not become large.

Fig. 5 shows an example in which the imaging optical element 4b of Embodiment 2 is applied to an original reading apparatus. Constituent parts in Fig. 5 are substantially similar to those in Fig. 2. The reference character 3C designates a mirror. In Fig. 5, the conventional imaging lens comprised of a plurality of lenses can be replaced by the imaging optical element 4b comprising a few constituents. The imaging optical element 4b is of a construction free of the occurrence of chromatic aberration and can therefore easily constitute an integral carriage type optical system capable of effecting color reading free of color misregister.

Fig. 6 shows aberrations at five points (image heights) in the line direction of the line sensor in Embodiment 2. In Fig. 6, X is representative of the height on the surface of the original.

Fig. 7 is a cross-sectional view of the essential portions of Embodiment 3 of the imaging optical element 4c of the present invention. The imaging optical element of Embodiment 3 is such that reflecting surfaces are six surfaces (R3 to R8) and the medium between adjacent reflecting surfaces is air. Accordingly, the imaging optical element 4c is

of a construction in which chromatic aberration does not occur. By an even number of times of reflection, the direction of the exit ray becomes substantially opposite to the direction of the incident ray.

5           The imaging optical element 4c of Fig. 7 is of an arrangement in which, in succession from the original surface 8 side, the surface R3 is a plus deflecting surface, the surface R4 is a plus deflecting surface, the surface R5 is a minus  
10   deflecting surface, the surface R6 is a minus deflecting surface, the surface R7 is a plus deflecting surface, and the surface R8 is a plus deflecting surface. As the result, the direction of the exit reference axis ray is substantially opposite  
15   to the direction of the incident reference axis ray. The arrangement of the deflecting surfaces is made such that a set in which the plus deflecting surfaces continue and a set in which the minus deflecting surfaces continue are alternately arranged, whereby  
20   the optical path travels in a direction substantially orthogonal to the incident ray and therefore, the imaging optical element 4c can assume a spatially efficient disposition.

          In Embodiment 3, as in Embodiment 1, the image  
25   of the original is designed not to be intermediately imaged in the imaging optical element 4c, but to be directly formed on the line sensor 5 so that the

curvature of each off-axial reflecting surface can be constructed gently. Further, the stop SP is disposed near the center of the optical path of the imaging optical element 4c so that the effective beams on the incidence surface R2 and exit surface R9 of the imaging optical element 4c may not become large.

Fig. 8 shows an example in which the imaging optical element 4c of Embodiment 3 is applied to an original reading apparatus. Constituent parts in Fig. 8 are substantially similar to those in Fig. 2. In Fig. 8, the imaging optical element 4c is constructed such that the exit ray emerges in a direction opposed to the direction of the incident ray, and this corresponds to the optical path being bent twice, and as in the original reading apparatus of Fig. 2, the reflecting mirrors can be decreased relative to the prior art. Further, as regards the disposition of the line sensor 5, a compact construction becomes possible.

Fig. 9 shows aberrations at five points (image heights) in the line direction of the line sensor in Embodiment 3. In Fig. 9, X is representative of the height on the surface of the original.

Figs. 10 to 14 are cross-sectional views of the essential portions of Embodiments 4 to 8 of the imaging optical element of the present invention.

The imaging optical elements of Figs. 10 to 14

have the imaging action chiefly by a plurality of reflecting surfaces. This is in a case where any of these imaging optical elements has five reflecting surfaces. The configurations of the imaging optical elements shown in Fig. 10 to Fig. 14 are appropriately selected in accordance with the construction of the reflecting mirrors provided in the original reading apparatus so as to accomplish more compact arrangement. Also even in a case where the number of the reflecting surfaces in an imaging optical element is six or more, several configurations of imaging optical elements are conceivable and therefore such configurations can be so selected as to conform to the construction of the original reading apparatus.

Fig. 15 is a cross-sectional view of the essential portions of Embodiment 9 of the imaging optical element of the present invention.

Fig. 16 shows an example in which the imaging optical element of Embodiment 9 is applied to an original reading apparatus.

The imaging optical element 4d of Embodiment 9 is such that reflecting surfaces comprise five surfaces (R3, R4, R6 to R8) and the medium between adjacent reflecting surfaces is air. Accordingly, the imaging optical element 4d is of a construction in which chromatic aberration does not occur.

The imaging optical element 4d of Fig. 15 is of

an arrangement in which, in succession from the original surface 8 side, the surface R3 is a plus deflecting surface, the surface R4 is a minus deflecting surface, the surface R6 is a plus  
5 deflecting surface, the surface R7 is a minus deflecting surface, and the surface R8 is a minus deflecting surface. By this construction, a beam emerging from a reflecting mirror 3b is bent toward the first reflecting mirror side in the imaging  
10 optical element 4d, whereafter the beam is made to emerge in a direction opposite to the reflecting mirror.

That is, by an odd number of times of reflection, the direction of the exit reference axis ray becomes  
15 substantially perpendicular to the direction of the incident reference axis ray. The beam emerging from the two reflecting mirrors 3a and 3b for repetitively bending the optical path is imaged and is bent in a direction perpendicular to the direction of incidence  
20 so as to travel along the optical path in the imaging optical element 4d in a direction opposite to the reflecting mirror, whereby a spatially efficient disposition can be assumed.

In Embodiment 9, as in Embodiment 1, the  
25 original image is designed not to be intermediately imaged in the imaging optical element 4d, but to be directly formed on the line sensor 5 to thereby make the curvature of each off-axial reflecting surface



gentle. Further, the stop SP is disposed near the center of the optical path of the imaging optical element 4d so that the effective beams on the incidence surface R2 and exit surface R9 of the  
5 imaging optical element may not become large. As shown, the imaging optical element 4d has the action of bending the optical path and therefore, an integral carriage type scanning type image reading  
10 apparatus can be realized by a simple construction comprising only two reflecting mirrors and an imaging optical element.

Fig. 17 is a cross-sectional view of the essential portions of Embodiment 10 of the imaging optical element of the present invention.

15 Fig. 18 shows an example in which the imaging optical element of Embodiment 10 is applied to an original reading apparatus.

The imaging optical element 4e of Embodiment 10 is such that reflecting surfaces comprise five  
20 surfaces (R3, R4, R6 to R8) and the medium between adjacent reflecting surfaces is air. Accordingly, the imaging optical element 4e is of a construction in which chromatic aberration does not occur.

The imaging optical element 4e of Fig. 17 is of  
25 an arrangement in which, in succession from the original surface 8 side, the surface R3 is a minus deflecting surface, the surface R4 is a plus

deflecting surface, the surface R6 is a plus  
deflecting surface, the surface R7 is a minus  
deflecting surface, and the surface R8 is a plus  
deflecting surface. By this construction, the beam  
5 emerging from the reflecting mirror 3b is linearly  
downwardly directed in the imaging optical element 4e,  
and thereafter emerges toward the reflecting mirror  
side.

That is, by an odd number of times of reflection,  
10 the direction of the exit reference axis ray is  
substantially perpendicular to the direction of the  
incident reference axis ray. The beam emerging from  
the two reflecting mirrors 3a and 3b for repetitively  
bending the optical path is imaged by the imaging  
15 optical element 4e, and the optical path is bent in a  
direction substantially orthogonal to the direction  
of incidence so as to travel toward the reflecting  
mirrors, whereby a spatially efficient disposition  
can be assumed.

20 In Embodiment 10, as in Embodiment 1, the  
original image is designed not to be intermediately  
imaged in the imaging optical element 4e, but to be  
directly formed on the line sensor 5 so that the  
curvature of each off-axial reflecting surface can be  
25 made gentle. Further, the stop SP is disposed near  
the center of the optical path of the imaging optical  
element 4e so that the effective beams on the

incidence surface R2 and exit surface R9 of the  
imaging optical element 4e may not become large. As  
shown, the imaging optical element 4e has the action  
of bending the optical path and therefore, an  
5 integral carriage type scanning type image reading  
apparatus can be realized by a simple construction  
comprising only two reflecting mirrors and the  
imaging optical element 4e.

Fig. 19 is a cross-sectional view of the  
10 essential portions of Embodiment 11 of the imaging  
optical element of the present invention.

Fig. 20 is an example in which the imaging  
optical element of Embodiment 11 is applied to an  
original reading apparatus.

15 The imaging optical element 4f of Embodiment 11  
is such that reflecting surfaces comprise six  
surfaces (R3 to R5, R7 to R9). Also, the medium  
between adjacent reflecting surfaces in the imaging  
optical element 4f is air. Accordingly, the imaging  
20 optical element 4f is of a construction in which  
chromatic aberration does not occur.

The imaging optical element 4f of Fig. 19 is of  
an arrangement in which, in succession from the  
original surface 8 side, the surface R3 is a plus  
25 deflecting surface, the surface R4 is a plus  
deflecting surface, the surface R5 is a minus  
deflecting surface, the surface R7 is a plus

deflecting surface, the surface R8 is a plus  
deflecting surface, and the surface R9 is a minus  
deflecting surface. In Fig. 20, the beam emerging  
from the reflecting mirror 3a has its optical path  
5 bent in the imaging optical element 4f, and  
thereafter is substantially linearly downwardly  
directed and emerges.

That is, the direction of the reference axis ray  
emerging from the imaging optical element 4f is  
10 substantially opposite to the direction of the  
incident reference axis ray. The beam emerging from  
two reflecting mirrors 3a and 3b for repetitively  
bending the optical path is imaged by the imaging  
optical element 4f, and the optical path is reversed  
15 and bent so as to travel downwardly, whereby a  
spatially efficient disposition can be assumed.

In Embodiment 11, as in Embodiment 1, the  
original image is designed not to be intermediately  
imaged in the imaging optical element 4f, but to be  
20 directly formed on the line sensor 5, and the  
curvature of each off-axial reflecting surface is  
made gentle. Further, the stop SP is disposed near  
the center of the optical path of the imaging optical  
element 4f so that the effective beams on the  
25 incidence surface R2 and exit surface R10 of the  
imaging optical element 4f may not become large. As  
shown, the imaging optical element has the action of

bending the optical path and therefore, an integral carriage type image reading apparatus can be realized by a simple construction comprising only the two reflecting mirrors 3a and 3b and the imaging optical element 4f. In this construction, the frequency of reflection of the beam by the reflecting mirror 3b can be decreased and therefore, the reflecting mirror 3b can be made small.

The above-described imaging optical elements 4d to 4f use reflecting surfaces which are free-form surfaces to thereby more shorten the distance between the original surface and the imaging optical element than in the conventional imaging optical system, thereby realizing the construction of an integral carriage type optical system.

Figs. 21A to 21C are cross-sectional views of the essential portions of Embodiment 12 of the imaging optical element of the present invention. The configuration of the imaging optical element of the present embodiment is the same as that of Embodiment 10 of Fig. 17.

Fig. 22 shows an example in which the imaging optical element of Embodiment 12 is applied to an original reading apparatus.

The imaging optical element of Figs. 21A to 21C has five off-axial reflecting surfaces (R3, R4, R6 to R8) differing in the direction of the incident ray of

the reference axis ray and the direction of the exit ray thereof from one another and having curvatures and has the function of imaging the original surface 8 on the line sensor 5. The medium between adjacent reflecting surfaces is air. Accordingly, the imaging optical element 4g is of a construction in which chromatic aberration does not occur. Each off-axial reflecting surface adopts a construction for bending the optical path in a cross section perpendicular to the line direction of the line sensor 5, i.e., the sub scanning cross section.

The imaging optical element 4g of Figs. 21A to 21C is of an arrangement in which, in succession from the original surface 8 side, the surface R3 is a minus deflecting surface, the surface R4 is a plus deflecting surface, the surface R6 is a plus deflecting surface, the surface R7 is a minus deflecting surface, and the surface R8 is a plus deflecting surface. As the result, the direction of the exit reference axis ray is substantially perpendicular to the direction of the incident reference axis ray.

In Figs. 21A to 21C, the stop SP is disposed between the second reflecting surface R4 and the third reflecting surface R6 intersecting with each other. Fig. 21A shows the optical path of a cross section perpendicular to the line direction of the

line sensor, i.e., the sub scanning cross section,  
and Fig. 21B shows the optical path of a cross  
section parallel to the line direction of the line  
sensor, i.e., the main scanning cross section. Fig.

5 21C shows a perspective view of the aforementioned  
optical paths.

In the imaging optical element 4g, the image on  
the original surface is designed not to be  
intermediately imaged in the imaging optical element,  
10 but to be directly imaged on the line sensor 5 after  
having emerged from the imaging optical element.  
Thereby the curvature of each off-axial reflecting  
surface can be made gentle and therefore, it becomes  
easy to suppress aberrations occurring in each  
15 reflecting surface. However, in the construction of  
adjacent reflecting surfaces, to construct them so as  
not to mutually intercept the optical path, it is  
unavoidable to secure the spacing between the  
adjacent surfaces large to a certain extent, but  
20 because of the construction in which the image on the  
original surface is not intermediately imaged in the  
imaging optical element, in the line direction of the  
line sensor, the beam widens as it goes away from the  
stop.

25 In the present embodiment, the stop SP is set  
near the center of the optical path of the imaging  
optical element so that the effective beams on the

incidence surface and exit surface of the imaging optical element may not become large in the main scanning direction. A beam is always obliquely incident on and reflected by an off-axial reflecting surface and therefore asymmetrical aberration occurs and thus, basically it is preferable to adopt a construction in which the asymmetrical aberration is offset.

So, in the present embodiment, the off-axial reflecting surfaces disposed before and behind the stop S constitute a set of off-axial reflecting surfaces intersecting with each other so as to become substantially symmetrical with respect to the stop. Further, in the construction, the off-axial reflecting surfaces adjacent to the set of off-axial reflecting surfaces intersecting with each other cannot help assuming a disposition parallel to the off-axial reflecting surfaces intersecting with each other, and the adjacent off-axial reflecting surfaces adopt a construction in which they intersect with each other. Accordingly, such disposition of the stop enables the stop to be constructed integrally with one of the off-axial reflecting surfaces intersecting with each other and the off-axial reflecting surface adjacent thereto.

In Fig. 22, the reference numeral 2 designates an original supporting glass table, the reference



characters 3a and 3b denote first and second reflecting mirrors, the reference character 4g designates the imaging optical element, and the reference numeral 5 denotes the line sensor comprised of a CCD or the like.

The original 8 placed on the original supporting glass table 2 is imaged on the line sensor 5 by the imaging optical element 4g and one line of the original can be read. In order to construct the original reading apparatus compactly, the optical path is folded by the first and second reflecting mirrors 3a and 3b. The imaging optical element 4g also contributes to folding the optical path. By using the imaging optical element 4g, the original reading apparatus of an integral carriage type optical system can be comprised of a few optical parts comprising the two reflecting mirrors and the imaging optical element.

As compared with the conventional construction, the optical path is bent substantially at a right angle by only the imaging optical element, and this corresponds to the adoption of a construction including a mirror in an imaging optical system, and the image reading apparatus can be simplified in construction. This integral carriage type optical system scans in a direction perpendicular to the line direction of the line sensor, i.e., the sub scanning

direction, to thereby two-dimensionally read the original surface.

Fig. 23 is a cross-sectional view of the essential portions of Embodiment 13 of the imaging optical element of the present invention. The configuration of the imaging optical element of the present embodiment is the same as that of Embodiment 10 of Fig. 17.

Fig. 24 shows an example in which the imaging optical element of Embodiment 13 is applied to an original reading apparatus.

The imaging optical element 4h of the present embodiment has five off-axial reflecting surfaces (R3, R4, R6 to R8), and the medium between adjacent reflecting surfaces is air. Accordingly, this imaging optical element is of a construction in which chromatic aberration does not occur.

The imaging optical element 4h is of an arrangement in which, in succession from the original surface 8 side, the surface R3 is a plus deflecting surface, the surface R4 is a minus deflecting surface, the surface R6 is a minus deflecting surface, the surface R7 is a plus deflecting surface, and the surface R8 is a plus deflecting surface. The direction of the reference axis ray emerging from the imaging optical element 4h is substantially perpendicular to the direction of the incident

reference axis ray. In this construction, the stop SP is disposed between the second reflecting surface R4 and the third reflecting surface R6 located to be intersected with each other. The stop SP is disposed  
5 near the center of the optical path of the imaging optical element 4h and therefore, the effective beams on the incidence surface and exit surface of the imaging optical element do not become large.

Basically it is preferable to adopt a  
10 construction in which asymmetrical aberration is cancelled and therefore, the off-axial reflecting surfaces disposed before and behind the stop SP constitute a set of off-axial reflecting surfaces intersecting with each other so as to be  
15 substantially symmetrical with respect to the stop SP.

Fig. 25 is a cross-sectional view of the essential portions of Embodiment 14 of the imaging optical element of the present invention. The configuration of the imaging optical element of the  
20 present embodiment is the same as that of Embodiment 1 of Figs. 1A and 1B.

Fig. 26 shows an example in which the imaging optical element of Embodiment 14 is applied to an original reading apparatus.

25 The imaging optical element 4i has five reflecting surfaces (R3 to R7), and the medium between adjacent reflecting surfaces is air.

Accordingly, the imaging optical element 4i is of a construction in which chromatic aberration does not occur. The imaging optical element 4i is of an arrangement in which, in succession from the original  
5 surface 8 side, the surface R3 is a plus deflecting surface, the surface R4 is a plus deflecting surface, the surface R5 is a minus deflecting surface, the surface R6 is a minus deflecting surface, and the surface R7 is a plus deflecting surface. By this  
10 construction, the reference axis ray emerging from the imaging optical element 4i emerges in a direction substantially orthogonal to the direction of incidence. In this construction, the stop SP is disposed between the third reflecting surface R5 and  
15 the fourth reflecting surface R6 intersecting with each other.

Further, the stop SP is disposed near the center of the optical path of the imaging optical element 4i so that the effective beams on the incidence surface  
20 and exit surface of the imaging optical element may not become large. Basically it is preferable to adopt a construction in which an asymmetrical aberration is cancelled and therefore, the off-axial reflecting surfaces disposed before and behind the  
25 stop constitute a set of off-axial reflecting surfaces intersecting with each other so as to be substantially symmetrical with respect to the stop.

Fig. 27 is a cross-sectional view of the essential portions of Embodiment 15 of the imaging optical element of the present invention. The configuration of the imaging optical element of the present embodiment is the same as that of Embodiment 3 of Fig. 7.

Fig. 28 shows an example in which the imaging optical element of Embodiment 15 is applied to an original reading apparatus.

10 The imaging optical element 4j has six reflecting surfaces (R3 to R5, R7 to R9). It is an imaging optical element in which the medium between adjacent reflecting surfaces is air. Accordingly, the imaging optical element 4j is of a construction 15 in which chromatic aberration does not occur. The imaging optical element 4j is of an arrangement in which, in succession from the original surface 8 side, the surface R3 is a plus deflecting surface, the surface R4 is a plus deflecting surface, the surface 20 R5 is a minus deflecting surface, the surface R7 is a minus deflecting surface, the surface R8 is a plus deflecting surface, and the surface R9 is a plus deflecting surface. By this construction, the incident beam is substantially linearly downwardly 25 directed in the imaging optical element, whereafter the direction of the reference axis ray emerging by an even number of times of reflection is

substantially opposite to the direction of the incident reference axis ray.

The original image is designed not to be intermediately imaged in the imaging optical element, but to be directly formed on the line sensor 5 so that the curvature of each off-axial reflecting surface can be made gentle. Further, the stop SP is disposed between the third reflecting surface R5 and the fourth reflecting surface R7 located to be intersected with each other. Since the stop SP is near the center of the optical path of the imaging optical element 4j, the effective beams on the incidence surface and exit surface of the imaging optical element 4j do not become large. Basically it is preferable to adopt a construction in which an asymmetrical aberration is cancelled and therefore, a set of off-axial reflecting surfaces intersecting with each other are designed such that the off-axial reflecting surfaces disposed before and behind the stop become substantially symmetrical with respect to the stop.

Fig. 29 is a cross-sectional view of the essential portions of Embodiment 16 of the imaging optical element of the present invention.

Fig. 30 shows an example in which the imaging optical element of Embodiment 16 is applied to an original reading apparatus.

The imaging optical element 4k has six reflecting surfaces (R3 to R5, R7 to R9). It is an imaging optical element in which the medium between adjacent reflecting surfaces is air. Accordingly, 5 the imaging optical element 4k is of a construction in which chromatic aberration does not occur. The imaging optical element 4k is of an arrangement in which, in succession from the original surface 8 side, the surface R3 is a plus deflecting surface, the 10 surface R4 is a plus deflecting surface, the surface R5 is a minus deflecting surface, the surface R7 is a minus deflecting surface, the surface R8 is a plus deflecting surface, and the surface R9 is a minus deflecting surface. By this construction, the 15 incident beam is substantially linearly downwardly directed in the imaging optical element, whereafter the direction of the reference axis ray emerging by even number of times of reflection is substantially the same direction as the direction of the incident 20 reference axis ray.

The original image is designed not to be intermediately imaged in the imaging optical element, but to be directly formed on the line sensor 5 so that the curvature of each off-axial reflecting 25 surface can be made gentle. Further, the stop SP is disposed between the third reflecting surface R5 and the fourth reflecting surface R7 located to be

intersected with each other. Since the stop SP is near the center of the optical path of the imaging optical element, the effective beams on the incidence surface and exit surface of the imaging optical element do not become large. Basically it is preferable to adopt a construction in which an asymmetrical aberration is cancelled and therefore, a set of off-axial reflecting surfaces intersecting with each other are designed such that the off-axial reflecting surfaces disposed before and behind the stop SP become substantially symmetrical with respect to the stop. The construction of the original reading apparatus is basically the same as that of Embodiment 1.

Fig. 34 is a cross-sectional view of the essential portions of Embodiment 17 of the imaging optical element of the present invention.

Fig. 36 shows an example in which the imaging optical element of Embodiment 17 is applied to an image reading apparatus.

In the imaging optical element 4 of Embodiment 17, the direction of the exit surface R11 relative to the incidence surface R3 for the reference axis ray is the same, and only off-axial reflecting surfaces having curvatures are comprised of six surfaces (R4 to R6, R8 to R10). The medium between adjacent reflecting surfaces is air, and basically the imaging



optical element is of a hollow construction in which chromatic aberration does not occur. By an even number of times of reflection, the direction of the incident ray and the direction of the exit ray become  
5 substantially the same directions.

The imaging optical element 4 of Fig. 34 is of an arrangement in which, in succession from the original surface 8 side, the surface R4 is a plus deflecting surface, the surface R5 is a plus  
10 deflecting surface, the surface R6 is a minus deflecting surface, the surface R8 is a plus deflecting surface, the surface R9 is a minus deflecting surface, and the surface 10 is a minus deflecting surface.

15 The surface R10 most adjacent to the exit side is disposed more adjacent to the original side on the incidence reference axis than the surface R4 most adjacent to the incidence side. By this disposition, the optical path emerging from the element 4 and  
20 leading to the imaging position, i.e., the so-called back focus portion, can be disposed below and substantially in parallel to a portion in which the incident light comes to the surface R4, and it is possible to assume a spatially efficient disposition.

25 Further, basically it is preferable to adopt a construction in which an asymmetrical aberration is cancelled and therefore, the off-axial reflecting

surfaces disposed before and behind the stop SP are of a construction in which the surface R6 is minus, whereas the surface R8 is plus, and the surface R5 is plus, whereas the surface R9 is minus, and the  
5 surface R4 is plus, whereas the surface R10 is minus, and when rotated by  $180^\circ$  about the stop, they become the same.

The beam travelling from the surface R4 toward the surface R5 is converged to thereby make the off-  
10 axial reflecting surfaces subsequent to the surface R4 small. Further, at least one of these off-axial reflecting surfaces is given the effect of cutting infrared light, whereby the black portion of a color image can be prevented from becoming reddish. As an  
15 example of the method of cutting infrared light, mention may be made of making an off-axial reflecting surface by evaporation-depositing or dipping dichroic film.

In Fig. 36, the reference numeral 2 designates  
20 an original supporting glass table, the reference characters 3a, 3b and 3c denote first, second and third reflecting mirrors, the reference numeral 4 designates the imaging optical element, and the reference numeral 5 denotes a line sensor comprised  
25 of a CCD or the like. An original 8 placed on the original supporting glass table 2 is imaged on the line sensor 5 by the imaging optical element 4,

whereby one line of the original can be read. In order to construct the original reading apparatus compactly, the optical path is folded by the first, second and third reflecting mirrors 3a, 3b and 3c.

5 As compared with the prior art, it is not necessary to dispose a lens in parallel to and below the mirrors and therefore, the imaging optical element can be made thin in the direction of depth (the direction vertical to the plane of the drawing sheet  
10 of Fig. 36). Further, the CCD or the like is disposed in the sub scanning direction and therefore, there is not the projection of a CCD substrate or the like in the direction of depth and the element can be made thin.

15 The imaging optical element of the present invention can be applied to optical apparatuses such as a color copier, a monochrome copier and an image scanner. Particularly it is best suited for a color digital copier of which bright F number and a high  
20 quality of image free of color misregister are required.

In the embodiments of the present invention, NA on the incidence side is made the same so that on the line sensor, the performance in a cross-sectional  
25 direction perpendicular to the line direction of the line sensor, i.e., the subscanning direction, and the performance in a direction parallel to the line

direction, i.e., the main scanning direction, may be substantially the same. In order to realize this, in the stop, the aperture width in a cross section perpendicular to the line direction of the line  
5 sensor and the aperture width in a direction parallel to the line direction are set so as to differ from each other. This is because the off-axial reflecting surfaces basically differ in curvature in the azimuth direction from each other and therefore the way in  
10 which the ray passes through the imaging optical element becomes asymmetrical.

Since it is necessary to dispose the asymmetrical stop with its direction made coincident with the direction of the off-axial reflecting  
15 surfaces, it is preferable that the off-axial reflecting surfaces proximate to the stop and the stop be constructed integrally with each other.

The construction of the present invention is applicable to a color copier, a monochrome copier and  
20 an image scanner.

According to each of the above-described embodiment, in an image reading apparatus for reading color and monochromatic image information by a line sensor and an imaging optical system, the imaging  
25 optical system is constituted by an imaging optical element comprising a plurality of off-axial reflecting surfaces having curvatures, whereby there

is realized an integral carriage type optical system which can effect highly definite image reading free of color misregister in the case of a color image and is of a compact construction.

5       Also, according to each of the above-described embodiments, in a color image reading apparatus for reading an original by a line sensor and an imaging optical system, a reading optical system constituted by an imaging optical element comprising a reflecting  
10 mirror for reflecting a reference axis ray a plurality of times and a plurality of off-axial reflecting surfaces having curvatures can realize an integral carriage type optical system by a simple construction. Further, the imaging optical element  
15 is comprised substantially of reflecting surfaces and therefore, the integral type optical system can realize highly definite image reading free of color misregister.

      Also, according to each of the above-described  
20 embodiments, in a color and monochrome image reading apparatus for reading image information by a line sensor and an imaging optical system, the imaging optical system is constituted by an imaging optical element comprising a plurality of off-axial  
25 reflecting surfaces having curvatures and the reflecting surfaces and stop of the imaging optical element are appropriately constructed, whereby there

can be realized an integral carriage type optical system of high performance which can effect highly definite image reading free of color misregister in the case of a color image.

5           In order to clarify the constructions and the meanings of the numerical values of the embodiments of the imaging optical element of the present invention, the off-axial optical system used herein and the reference axis which provides a skeleton  
10           thereof will be defined as follows.

#### Definition of the Reference Axis

          Generally the optical path of a ray of a reference wavelength from an object surface to an image plane which provides a reference is defined as  
15           the reference axis in the optical system. This leaves ambiguity to the way of choosing a ray which provides a reference and therefore, usually the reference ray, i.e., the reference axis, is set by two fundamental rules shown below.

20           When an axis having, if partially, symmetry exists in an optical system, and aberrations can be arranged in order with good symmetry, a ray passing on the axis having symmetry is regarded as the reference ray.

25           When generally a symmetry axis does not exist in an optical system or a symmetry axis partially exists but aberrations can be arranged in order with good

symmetry, among rays leaving the center of an object surface (the center of a range to be photographed or observed), a ray passing through the optical system in the order of the designated surfaces of the optical system, and passing through the center of a stop defined in the optical system is set as the reference ray.

It is usually the case that the reference axis defined in this manner assumes a bent shape.

#### 10 Definition of the Off-axial Optical System

A curved surface of which the surface normal does not coincide with the reference axis at a point whereat the reference axis defined as described above is defined as an off-axial curved surface, and an optical system including the off-axial curved surface is defined as an off-axial optical system. (However, when the reference axis is simply bent by a planar reflecting surface, the surface normal again does not coincide with the reference axis, but yet the planar reflecting surface does not spoil the symmetry of aberration and therefore it is excluded from the subject of the off-axial optical system.)

While in the embodiments of the present invention, the reference axis which provides the reference of the optical axis has been set as described above, the way of determining the axis which provides the reference of the optical system

can be selected by adopting an axis convenient in optical design, arranging aberrations in order or expressing the shape of each surface constituting the optical system.

5           Generally, however, the route of a ray passing through the center of an image plane or an observation plane, and one of the center of a stop or an entrance pupil or an exit pupil or the first surface of the optical system and the center of the  
10 last surface is set as the reference axis which provides the reference of the optical system.

That is, in the embodiments of the present invention, the route along which a ray passing through the central point of the line sensor 5  
15 (imaging plane) to the center of the image plane (reference axis ray) is reflected by the reflecting surfaces is set as the reference axis. The order of the surfaces is set to the order in which the reference axis ray is subjected to reflection.

20           Accordingly, the reference axis finally arrives at the center of the image plane while having its direction changed along the order of the surfaces in accordance with the law of reflection.

Tilted surfaces constituting the optical system  
25 of each embodiment of the present invention are all basically tilted in the same plane. So, the axes of the absolute coordinate system are defined as follows.



(See Fig. 31)

Z-axis: reference axis passing through the origin and going toward the second surface

Y-axis: straight line passing through the  
5 origin and counter-clockwisely forming an angle of  $90^\circ$  with respect to the Z-axis in the tilt plane (the plane of the drawing sheet of Fig. 31)

X-axis: straight line passing through the origin and perpendicular to the Z- and Y- axis (straight  
10 line perpendicular to the plane of the drawing sheet of Fig. 31)

Also, to represent the surface shape of the  $i$ th surface constituting the optical system, it is easier to understand in recognizing the shape to set a local  
15 coordinate system in which a point at which the reference axis and the  $i$ th surface intersect with each other, and represent the surface shape of that surface by the local coordinate system than to represent the shape of that surface by the absolute  
20 coordinate system and therefore, in the embodiments indicating the construction data of the present invention, the surface shape of the  $i$ th surface is represented by the local coordinate system.

Also, the tilt angle of the  $i$ th surface in YZ  
25 plane is represented by an angle  $\theta_i$  (unit being  $^\circ$ ) in which a counter-clockwise direction relative to the Z-axis of the absolute coordinate system is positive.

Consequently, in the embodiments of the present invention, the origin of the local coordinates of each surface is on YZ plane in Fig. 31.

Also, there is not decentering of the surface in  
5 XZ and XY planes. Further, the y- and z-axis of the local coordinates (x, y, z) of the ith surface are inclined by an angle  $\theta_i$  in YZ plane with respect to the absolute coordinate system (X, Y, Z), and specifically are set as follows.

10 z-axis: straight line passing through the origin of the local coordinates, and counter-clockwisely forming an angle  $\theta_i$  in YZ plane with respect to the Z direction of the absolute coordinate system

y-axis: straight line passing through the origin  
15 of the local coordinates, and counter-clockwisely forming an angle of  $90^\circ$  in YZ plane with respect to z direction

x-axis: straight line passing through the origin of the local coordinates, and perpendicular to YZ  
20 plane

Also, the imaging optical element in each embodiment of the present invention has a rotation-asymmetrical aspherical surface and the shape thereof is indicated by the following expression:

25 
$$z = C_{02}Y^2 + C_{20}X^2 + C_{03}Y^3 + C_{21}X^2Y + C_{04}Y^4 + C_{22}X^2Y^2 + C_{40}X^4 + C_{05}Y^5 + C_{23}X^2Y^3 + C_{41}X^4Y + C_{06}Y^6 + C_{24}X^2Y^4 + C_{42}X^4Y^2 + C_{60}X^6$$

The spherical surface is of a shape represented

by the following expression:

$$z = ((x^2+y^2)/r_i) / (1+(1-(x^2+y^2)/r_i)^{1/2})$$

The above-mentioned curved surface expression has only a term of an even number order regarding x and therefore, the curved surface prescribed by the above-mentioned curved surface expression is of a plane-symmetrical shape having yz plane as a symmetrical plane. Further, when the following conditions are satisfied, it represents a shape symmetrical with respect to xz plane.

$$C_{03} = C_{21} = 0$$

$$C_{02} = C_{20}C_{04} = C_{40} = C_{22}/2$$

$$C_{05} = C_{23} = C_{41} = 0$$

$$C_{60} = C_{06} = C_{24}/3 = C_{42}/3$$

When the above-mentioned conditions are satisfied, it represents a rotation-symmetrical shape. When the above-mentioned conditions are not satisfied, it represents a rotation-asymmetrical shape.

Also, all of the embodiments of the optical system are not coaxial optical systems and therefore, it is difficult to directly calculate a focal length based on a paraxial theory. So, use is made of a converted focal length  $f_{eq}$  by the following definition:

$$f_{eq} = h_1 / \tan(a_k')$$

In definition, when the number of the reflecting surfaces is an odd number, the sign of the focal

length is expressed as being opposite to the ordinary sign.

Here,

5  $h_1$ : the incidence height of a ray parallel to the reference axis on the first surface and incident infinitely near the reference axis,

$a_k'$ : an angle the ray forms with respect to the reference axis when it emerges from the last surface.

10 Next, in numerical value embodiments, it is to be understood that the sign of the radius of curvature  $R_i$  is minus when the center of curvature is on the first surface  $R_1$  side along the reference axis indicated by dot-and-dash line travelling from the first surface  $R_1$  to the imaging plane, and is plus  
15 when the center of curvature is on the imaging plane side.

Also,  $D_i$  is a scalar amount representing the interval between the origins of the local coordinates between the  $i$ th surface and the  $(i+1)$ th surface, and  
20  $N_{di}$  and  $v_{di}$  are the refractive index and Abbe number, respectively, of the medium between the  $i$ th surface and the  $(i+1)$ th surface.

The effective dimension  $(X*Y)$  is the effective dimension in the X-axis direction and the Y-axis  
25 direction of the local coordinates of each surface.

Numerical value data will be shown below regarding Embodiments 1 to 3 and 9 to 17 of the present invention described above.

# Numerical Embodiment 1

Read Width of Original: 222, Imaging Magnification: -0.1653,  
NA at Original Side: 0.0187,  $f_{eq}$ : -34

i	Yi	Zi	$\theta_i$	Di	$N_{di}$	$\nu_{di}$	Effective Size (X*Y)	
1	0.00	-220.44	0.0	220.44	1.00000			Object Surface (Original Surface)
2	0.00	0.00	0.0	4.80	1.49171	57.4	23.1*9.4	Refracting Surface
3	0.00	4.80	45.0	9.00	1.49171	57.4	20.7*13.0	Reflecting Surface
4	-9.00	4.80	45.0	9.60	1.49171	57.4	14.8*12.8	Reflecting Surface
5	-9.00	-4.80	-45.0	10.40	1.49171	57.4	10.0*13.9	Reflecting Surface (Stop)
6	-19.40	-4.80	-45.0	8.40	1.49171	57.4	15.0*12.5	Reflecting Surface
7	-19.40	3.60	45.0	4.00	1.49171	57.4	18.3*11.3	Reflecting Surface
8	-23.40	3.60	0.0	27.42	1.49171	57.4	19.3*7.3	Refracting Surface
9	-50.82	3.60			1.00000			Image Plane (Sensor Surface)

## Aspherical Shape

### R2 Surface

$C_{02}=-2.9789e-3$	$C_{03}=1.0562e-4$	$C_{04}=1.7462e-4$
$C_{05}=-2.3567e-5$	$C_{06}=-8.7694e-6$	$C_{20}=-2.6345e-3$
$C_{21}=-1.9654e-4$	$C_{22}=2.0985e-5$	$C_{23}=-3.2325e-6$
$C_{24}=-1.5225e-6$	$C_{40}=-1.3607e-5$	$C_{41}=7.6570e-7$
$C_{42}=9.9798e-8$	$C_{60}=3.1988e-8$	

### R3 Surface

$C_{02}=-2.1480e-3$	$C_{03}=2.4400e-4$	$C_{04}=2.6765e-6$
$C_{05}=-5.6807e-7$	$C_{06}=-3.1410e-7$	$C_{20}=-1.9036e-3$
$C_{21}=9.0398e-5$	$C_{22}=3.8180e-6$	$C_{23}=-1.6067e-6$
$C_{24}=-1.2060e-9$	$C_{40}=-5.5316e-7$	$C_{41}=1.4369e-7$
$C_{42}=-3.0686e-9$	$C_{60}=5.2469e-9$	

### R4 Surface

$C_{02}=-6.3716e-3$	$C_{03}=2.3535e-4$	$C_{04}=-2.2599e-6$
$C_{05}=1.8392e-6$	$C_{06}=1.0760e-8$	$C_{20}=-4.4929e-3$
$C_{21}=3.8336e-4$	$C_{22}=2.5288e-5$	$C_{23}=-2.67715e-6$
$C_{24}=-2.2107e-7$	$C_{40}=-1.6080e-6$	$C_{41}=-1.4510e-7$
$C_{42}=2.6110e-8$	$C_{60}=-2.4164e-8$	

### R5 Surface

$C_{02}=-7.4735e-3$	$C_{03}=-7.3808e-5$	$C_{04}=-1.4600e-6$
$C_{05}=-2.2939e-7$	$C_{06}=-5.2718e-8$	$C_{20}=-8.7526e-3$
$C_{21}=-1.6764e-5$	$C_{22}=9.5058e-6$	$C_{23}=-1.2307e-7$
$C_{24}=-8.0893e-8$	$C_{40}=4.0064e-7$	$C_{41}=6.8219e-7$
$C_{42}=5.3009e-8$	$C_{60}=-1.1033e-8$	

$C_{02} = -2.2655e-3$   
 $C_{05} = -1.4458e-6$   
 $C_{21} = -3.6644e-4$   
 $C_{24} = -1.0209e-7$   
 $C_{42} = 4.0904e-8$

$$\begin{aligned}C_{04} &= -3.0938e-5 \\ C_{20} &= -1.0043e-3 \\ C_{23} &= 3.2807e-7 \\ C_{41} &= 1.0709e-6\end{aligned}$$

$C_{02} = -3.3233e-3$   
 $C_{05} = -2.4643e-6$   
 $C_{21} = -1.3299e-4$   
 $C_{24} = 3.3475e-7$   
 $C_{42} = -7.3342e-8$

$$\begin{aligned}C_{04} &= -1.1412e-5 \\ C_{20} &= -5.5907e-3 \\ C_{23} &= 1.4412e-6 \\ C_{41} &= -4.1994e-7\end{aligned}$$
$$\begin{aligned}C_{02} &= -2.0078e-2 \\C_{05} &= 2.7529e-5 \\C_{21} &= -3.8863e-4 \\C_{22} &= 5.5839e-6 \\C_{42} &= -3.1740e-7\end{aligned}$$
$$\begin{aligned} C_{04} &= 1.7886e-4 \\ C_{20} &= -1.6884e-2 \\ C_{23} &= -5.5015e-6 \\ C_{41} &= -4.7857e-6 \end{aligned}$$

# Numerical Embodiment 2

Read Width of Original: 222, Imaging Magnification: -0.1653,  
NA at Original Side: 0.0187,  $f_{eq}$ : 41.6

i	Yi	Zi	$\theta_i$	Di	N <sub>di</sub>	Effective Size (X*Y)	
1	0.00	-238.56	0.0	238.56	1.		Object Surface (Original Surface)
2	0.00	0.00	0.0	6.80	1.	37.6*16.8	Transmitting Surface
3	0.00	6.80	45.0	9.50	1.	35.6*16.8	Reflecting Surface
4	-9.50	6.80	-45.0	8.00	1.	18.6*12.5	Reflecting Surface
5	-9.50	14.80	-45.0	8.00	1.	8.1*9.0	Reflecting Surface (Stop)
6	-1.50	14.80	45.0	7.20	1.	15.9*9.4	Reflecting Surface
7	-1.50	22.00	45.0	7.20	1.	23.4*9.7	Reflecting Surface
8	-8.70	22.00	-45.0	5.00	1.	24.9*8.7	Reflecting Surface
9	-8.70	27.00	0.0	16.44	1.	28.1*5.1	Transmitting Surface
10	-8.70	43.44			1.		Image Plane (Sensor Surface)

## Aspherical Shape

### R3 Surface

$C_{02}=-5.7442e-3$	$C_{03}=2.4771e-4$	$C_{04}=-6.6994e-7$
$C_{05}=2.3519e-7$	$C_{06}=9.1306e-9$	$C_{20}=-8.0122e-3$
$C_{21}=1.4778e-4$	$C_{22}=-5.9973e-6$	$C_{23}=1.6237e-7$
$C_{24}=-1.9675e-8$	$C_{40}=2.6142e-8$	$C_{41}=4.7468e-10$
$C_{42}=9.6616e-11$	$C_{60}=-8.8382e-10$	

### R4 Surface

$C_{02}=-7.3438e-3$	$C_{03}=8.3463e-4$	$C_{04}=-1.0717e-5$
$C_{05}=3.9674e-7$	$C_{06}=-6.0573e-8$	$C_{20}=-9.9018e-3$
$C_{21}=8.4968e-5$	$C_{22}=-4.6718e-7$	$C_{23}=-2.5933e-6$
$C_{24}=1.9199e-7$	$C_{40}=-6.7688e-6$	$C_{41}=4.8523e-7$
$C_{42}=-4.6662e-8$	$C_{60}=-2.7055e-8$	

### R5 Surface

$C_{02}=-4.2699e-3$	$C_{03}=-3.8900e-4$	$C_{04}=4.4021e-5$
$C_{05}=-9.6222e-8$	$C_{06}=3.8576e-7$	$C_{20}=-3.9951e-3$
$C_{21}=-5.2587e-4$	$C_{22}=4.5333e-5$	$C_{23}=-4.1085e-6$
$C_{24}=3.4840e-7$	$C_{40}=-1.1388e-5$	$C_{41}=3.9818e-7$
$C_{42}=6.8919e-9$	$C_{60}=-1.5466e-9$	

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R6 Surface

$C_{02}=-6.8815e-3$	$C_{03}=-1.7608e-3$	$C_{04}=-9.0668e-5$
$C_{05}=-1.8681e-6$	$C_{06}=1.7803e-7$	$C_{20}=1.2113e-3$
$C_{21}=-8.6697e-4$	$C_{22}=-6.8378e-5$	$C_{23}=-3.3468e-6$
$C_{24}=-1.5663e-7$	$C_{40}=-1.0460e-5$	$C_{41}=-1.8794e-6$
$C_{42}=-1.3160e-7$	$C_{60}=-3.5402e-8$	

R7 Surface

$C_{02}=-7.3105e-3$	$C_{03}=-2.4918e-4$	$C_{04}=-3.9441e-6$
$C_{05}=1.3150e-6$	$C_{06}=-6.6461e-8$	$C_{20}=-1.1248e-2$
$C_{21}=-9.1503e-5$	$C_{22}=-1.5167e-5$	$C_{23}=9.0871e-8$
$C_{24}=1.9344e-7$	$C_{40}=2.2341e-6$	$C_{41}=-1.0184e-7$
$C_{42}=-4.0580e-8$	$C_{60}=6.0658e-9$	

R8 Surface

$C_{02}=1.5693e-3$	$C_{03}=4.7237e-4$	$C_{04}=3.4671e-5$
$C_{05}=4.9653e-6$	$C_{06}=-7.4511e-7$	$C_{20}=-5.1051e-3$
$C_{21}=5.9517e-5$	$C_{22}=-1.8425e-5$	$C_{23}=-1.0409e-6$
$C_{24}=1.3118e-7$	$C_{40}=5.1683e-7$	$C_{41}=-9.0297e-8$
$C_{42}=1.5252e-8$	$C_{60}=9.5374e-9$	

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Read Width of Original: 222, Imaging Magnification: -0.1653,  
NA at Original Side: 0.0187,  $f_{eq}$ : 36.7

i	Y <sub>i</sub>	Z <sub>i</sub>	θ <sub>i</sub>	D <sub>i</sub>	N <sub>di</sub>	Effective Size (X*Y)	
1	0.00	-211.00	0.0	211.00	1.		Object Surface (Original Surface)
2	0.00	0.00	0.0	5.00	1.	33.6*9.2	Transmitting Surface
3	0.00	5.00	45.0	10.30	1.	29.5*12.8	Reflecting Surface
4	-10.30	5.00	45.0	11.30	1.	18.3*12.0	Reflecting Surface
5	-10.30	-6.30	-45.0	11.50	1.	9.6*13.8	Reflecting Surface (Stop)
6	-21.80	-6.30	-45.0	12.50	1.	19.4*14.2	Reflecting Surface
7	-21.80	6.20	45.0	10.00	1.	27.8*13.9	Reflecting Surface
8	-31.80	6.20	45.0	6.00	1.	31.9*9.6	Reflecting Surface
9	-31.80	0.20	0.0	19.00	1.	32.4*5.6	Transmitting Surface
10	-31.80	-18.80			1.		Image Plane (Sensor Surface)

## Aspherical Shape

### R3 Surface

$C_{02}=-2.4010e-3$	$C_{03}=1.1320e-4$	$C_{04}=-8.3702e-7$
$C_{05}=8.2198e-7$	$C_{06}=-4.7624e-8$	$C_{20}=-9.0931e-4$
$C_{21}=1.0622e-4$	$C_{22}=-9.0082e-6$	$C_{23}=2.8992e-7$
$C_{24}=-1.5224e-8$	$C_{40}=-4.8672e-7$	$C_{41}=-3.9414e-8$
$C_{42}=3.9786e-9$	$C_{60}=-1.9739e-10$	

#### R4 Surface

$C_{02}=-5.7894e-3$	$C_{03}=8.0244e-4$	$C_{04}=-1.2590e-5$
$C_{05}=-2.3273e-6$	$C_{06}=-1.2782e-7$	$C_{20}=-4.0612e-3$
$C_{21}=3.8984e-4$	$C_{22}=-1.2270e-5$	$C_{23}=-1.3566e-6$
$C_{24}=-1.5134e-7$	$C_{40}=-4.6238e-6$	$C_{41}=-1.5878e-7$
$C_{42}=6.4425e-9$	$C_{60}=2.8316e-9$	

## R5 Surface

$C_{02}=-4.7063\text{e-}3$	$C_{03}=4.8880\text{e-}5$	$C_{04}=-4.9287\text{e-}6$
$C_{05}=2.5216\text{e-}7$	$C_{06}=-7.4539\text{e-}9$	$C_{20}=-7.3560\text{e-}3$
$C_{21}=1.4807\text{e-}4$	$C_{22}=1.1067\text{e-}5$	$C_{23}=-3.0590\text{e-}7$
$C_{24}=-4.7628\text{e-}8$	$C_{40}=1.3587\text{e-}6$	$C_{41}=1.7458\text{e-}7$
$C_{42}=1.4999\text{e-}8$	$C_{60}=5.5182\text{e-}10$	

## R8 Surface

$C_{02}=-2.1803e-3$	$C_{03}=1.2655e-4$	$C_{04}=-2.9430e-5$
$C_{05}=-1.0966e-6$	$C_{06}=6.5709e-8$	$C_{20}=2.0507e-3$
$C_{21}=8.0305e-5$	$C_{22}=-1.2759e-5$	$C_{23}=6.0378e-7$
$C_{24}=1.3627e-7$	$C_{40}=-2.0631e-6$	$C_{41}=8.3233e-8$
$C_{42}=-2.1609e-8$	$C_{60}=-1.7335e-10$	

Numerical Embodiment 9

Read Width of Original: 222, Imaging Magnification: -0.1649,  
NA at Original Side: 0.0187,  $f_{eq}$ : -38.8

i	Yi	Zi	$\theta_i$	Di	N <sub>di</sub>	Effective Size (X*Y)	
1	0.00	-217.50	0.0	227.50	1.		Object Surface (Original Surface)
2	0.00	0.00	0.0	5.00	1.	30.3*8.9	Transmitting Surface
3	0.00	5.00	45.0	9.50	1.	27.9*13.5	Reflecting Surface
4	-9.50	5.00	-45.0	5.00	1.	13.4*11.9	Reflecting Surface
5	-9.50	10.00	0.0	6.00	1.	8.2*9.0	Transmitting Surface (Stop)
6	-9.50	16.00	45.0	10.50	1.	15.6*14.1	Reflecting Surface
7	-20.00	16.00	-45.0	10.00	1.	22.9*12.2	Reflecting Surface
8	-20.00	26.00	-45.0	5.00	1.	28.5*12.6	Reflecting Surface
9	-15.00	26.00	0.0	25.00	1.	29.6*7.6	Transmitting Surface
10	10.00	26.00			1.		Image Plane (Sensor Surface)

Aspherical Shape

R3: Surface

$C_{02}$	=-2.3768e-3	$C_{03}$	=5.1145e-5	$C_{04}$	=-1.8547e-6
$C_{20}$	=-7.0111e-3	$C_{21}$	=1.8558e-4	$C_{22}$	=1.3075e-6
$C_{40}$	=-5.7256e-7				

R4: Surface

$C_{02}$	=-3.0863e-3	$C_{03}$	=1.2705e-4	$C_{04}$	=-7.8544e-6
$C_{20}$	=-1.2171e-2	$C_{21}$	=2.0905e-5	$C_{22}$	=2.5253e-6
$C_{40}$	=-9.7513e-6				

R6: Surface

$C_{02}$	=-4.3326e-3	$C_{03}$	=3.8979e-5	$C_{04}$	=-2.1266e-6
$C_{20}$	=-7.6579e-3	$C_{21}$	=-2.6482e-4	$C_{22}$	=1.1806e-5
$C_{40}$	=-5.1469e-6				

R7: Surface

$C_{02}$	=-3.2687e-3	$C_{03}$	=3.3262e-5	$C_{04}$	=4.5318e-6
$C_{20}$	=2.7881e-3	$C_{21}$	=-1.8228e-5	$C_{22}$	=9.3375e-6
$C_{40}$	=-1.2044e-6				

R8: Surface

$C_{02}$	=-5.3385e-3	$C_{03}$	=-1.2928e-5	$C_{04}$	=3.4083e-6
$C_{20}$	=-4.8503e-3	$C_{21}$	=4.9994e-5	$C_{22}$	=-5.3966e-6
$C_{40}$	=1.8097e-6				

Numerical Embodiment 10

Read Width of Original: 222, Imaging Magnification: -0.1647,  
NA at Original Side: 0.0187,  $f_{eq}$ : -37.9

i	Yi	Zi	$\theta_i$	Di	N <sub>di</sub>	Effective Size (X*Y)	
1	0.00	-233.54	0.0	233.54	1.		Object Surface (Original Surface)
2	0.00	0.00	0.0	5.00	1.	26.8*9.4	Transmitting Surface
3	0.00	5.00	-45.0	10.50	1.	22.3*13.4	Reflecting Surface
4	10.50	5.00	45.0	5.00	1.	15.2*11.1	Reflecting Surface
5	10.50	10.00	0.0	5.00	1.	9.7*8.3	Transmitting Surface (Stop)
6	10.50	15.00	45.0	9.00	1.	12.7*12.1	Reflecting Surface
7	1.50	15.00	-45.0	7.50	1.	17.6*9.0	Reflecting Surface
8	1.50	22.50	45.0	5.00	1.	24.5*8.1	Reflecting Surface
9	-3.50	22.50	0.0	16.17	1.	27.1*4.5	Transmitting Surface
10	-19.67	22.50			1.		Image Plane (Sensor Surface)

Aspherical Shape

R3 Surface

$$\begin{aligned} C_{02} &= -3.9970e-3 & C_{03} &= -5.1427e-5 & C_{04} &= -1.0984e-6 \\ C_{20} &= -3.0789e-5 & C_{21} &= -2.2585e-4 & C_{22} &= 1.6637e-6 \\ C_{40} &= 4.8584e-6 \end{aligned}$$

R4 Surface

$$\begin{aligned} C_{02} &= -5.4782e-3 & C_{03} &= -7.4478e-5 & C_{04} &= 9.7319e-6 \\ C_{20} &= 5.1369e-3 & C_{21} &= -3.6238e-4 & C_{22} &= -8.6823e-6 \\ C_{40} &= 6.2243e-7 \end{aligned}$$

R6 Surface

$$\begin{aligned} C_{02} &= -6.2734e-3 & C_{03} &= 3.8880e-5 & C_{04} &= 6.4718e-6 \\ C_{20} &= -6.5071e-3 & C_{21} &= 1.6088e-4 & C_{22} &= -5.8896e-6 \\ C_{40} &= -3.2072e-6 \end{aligned}$$

R7 Surface

$$\begin{aligned} C_{02} &= -2.3922e-3 & C_{03} &= -3.2812e-4 & C_{04} &= 7.5676e-8 \\ C_{20} &= -4.8178e-3 & C_{21} &= 3.7897e-4 & C_{22} &= -1.4111e-5 \\ C_{40} &= -9.2105e-6 \end{aligned}$$

R8 Surface

$$\begin{aligned} C_{02} &= -3.2644e-3 & C_{03} &= -5.1667e-4 & C_{04} &= 1.8927e-5 \\ C_{20} &= -4.2423e-3 & C_{21} &= -1.0882e-5 & C_{22} &= -2.0946e-5 \\ C_{40} &= 7.1399e-7 \end{aligned}$$

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Numerical Embodiment 11

Read Width of Original: 222, Imaging Magnification: -0.1749,  
NA at Original Side: 0.0187,  $f_{eq}$ : 38.4

i	Yi	Zi	$\theta_i$	Di	N <sub>di</sub>	Effective size (X*Y)	
1	0.00	-212.23	0.0	212.23	1.		Object Surface (Original Surface)
2	0.00	0.00	0.0	5.00	1.	34.4*8.9	Transmitting Surface
3	0.00	5.00	45.0	9.50	1.	31.1*13.0	Reflecting Surface
4	-9.50	5.00	45.0	9.00	1.	18.9*11.0	Reflecting Surface
5	-9.50	-4.00	-45.0	5.00	1.	14.3*11.5	Reflecting Surface
6	-14.50	-4.00	0.0	5.00	1.	9.3*7.3	Transmitting Surface (Stop)
7	-19.50	-4.00	45.0	9.00	1.	12.3*9.5	Reflecting Surface
8	-19.50	-13.00	45.0	7.50	1.	20.2*10.0	Reflecting Surface
9	-12.00	-13.00	-45.0	5.00	1.	23.0*7.3	Reflecting Surface
10	-12.00	-18.00	0.0	17.77	1.	26.2*4.0	Transmitting Surface
11	12.00	-35.77			1.		Image Plane (Sensor Surface)

Aspherical Shape

R3 Surface

$C_{02}=-3.5436e-3$	$C_{03}=7.0417e-5$	$C_{04}=-2.8147e-6$
$C_{20}=-1.4891e-3$	$C_{21}=4.0236e-5$	$C_{22}=5.2032e-8$
$C_{40}=2.7294e-8$		

R4 Surface

$C_{02}=-4.8426e-3$	$C_{03}=1.2702e-4$	$C_{04}=-5.7706e-6$
$C_{20}=-5.4450e-3$	$C_{21}=2.5363e-4$	$C_{22}=-2.9344e-6$
$C_{40}=-9.2465e-6$		

R5 Surface

$C_{02}=-4.1294e-3$	$C_{03}=1.9232e-4$	$C_{04}=-2.0532e-6$
$C_{20}=-1.0196e-2$	$C_{21}=1.9100e-4$	$C_{22}=4.1731e-6$
$C_{40}=-5.8741e-6$		

R7 Surface

$C_{02}=-3.4497e-3$	$C_{03}=3.3613e-4$	$C_{04}=2.3493e-6$
$C_{20}=-1.1953e-3$	$C_{21}=6.2801e-5$	$C_{22}=1.2506e-5$
$C_{40}=-1.5388e-6$		

R8 Surface

$C_{02}=-6.5017e-3$	$C_{03}=3.1224e-4$	$C_{04}=7.3823e-6$
$C_{20}=-6.3660e-3$	$C_{21}=1.0528e-4$	$C_{22}=-7.8242e-6$
$C_{40}=-1.5287e-6$		

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# R9 Surface

$C_{02}=-5.0330e-4$	$C_{03}=3.8280e-4$	$C_{04}=-1.2474e-5$
$C_{20}=-7.9714e-4$	$C_{21}=1.2684e-4$	$C_{22}=-2.8871e-5$
$C_{40}=-5.9100e-6$		

## Numerical Embodiment 12

Read Width of Original: 222, Imaging Magnification: -0.1653,  
NA at Original Side: 0.0187,  $f_{eq}$ : -38.0

i	Yi	Zi	$\theta_i$	Di	$N_{di}$	Effective Size (X*Y)	
1	0.00	-234.47	0.0	234.47	1.		Object Surface (Original Surface)
2	0.00	0.00	0.0	5.00	1.	26.5*9.3	Transmitting Surface
3	0.00	5.00	-45.0	10.50	1.	22.1*13.3	Reflecting Surface
4	10.50	5.00	45.0	5.00	1.	15.0*11.1	Reflecting Surface
5	10.50	10.00	0.0	5.00	1.	9.8*8.2	Transmitting Surface (Stop)
6	10.50	15.00	45.0	9.00	1.	12.8*11.8	Reflecting Surface
7	1.50	15.00	-45.0	7.50	1.	17.2*8.6	Reflecting Surface
8	1.50	22.50	45.0	5.00	1.	24.1*7.4	Reflecting Surface
9	-3.50	22.50	0.0	15.53	1.	26.9*4.0	Transmitting Surface
10	-19.03	22.50					Image Plane (Sensor Surface)

## Aspherical Shape

### R3' Surface

$C_{02}=-4.0198e-3$	$C_{03}=-4.3312e-5$	$C_{04}=1.6186e-6$
$C_{05}=-2.0989e-8$	$C_{06}=8.9768e-9$	$C_{20}=2.8439e-4$
$C_{21}=-1.5619e-4$	$C_{22}=2.2172e-6$	$C_{23}=2.2829e-7$
$C_{24}=3.9202e-8$	$C_{40}=4.0661e-6$	$C_{41}=1.4412e-7$
$C_{42}=2.2936e-8$	$C_{60}=5.7706e-10$	

### R4. Surface

$C_{02}=-5.4117e-3$	$C_{03}=-7.3877e-5$	$C_{04}=1.0743e-5$
$C_{05}=-2.4521e-8$	$C_{06}=1.1018e-8$	$C_{20}=5.2872e-3$
$C_{21}=-2.7535e-4$	$C_{22}=-5.4940e-6$	$C_{23}=8.5892e-8$
$C_{24}=3.7137e-8$	$C_{40}=-5.9045e-7$	$C_{41}=9.1078e-8$
$C_{42}=2.8573e-8$	$C_{60}=1.3710e-9$	

### R6 Surface

$C_{02}=-6.3295e-3$	$C_{03}=2.7750e-5$	$C_{04}=4.7126e-6$
$C_{05}=-1.2480e-9$	$C_{06}=4.0127e-9$	$C_{20}=-6.9688e-3$
$C_{21}=1.3190e-4$	$C_{22}=-1.0478e-5$	$C_{23}=-3.2445e-7$
$C_{24}=-2.8006e-10$	$C_{40}=-6.3309e-6$	$C_{41}=-1.9653e-7$
$C_{42}=-3.5731e-9$	$C_{60}=-1.6195e-8$	

$$\begin{aligned}C_{02} &= -2.3617e-3 \\ C_{05} &= 4.3632e-7 \\ C_{21} &= 2.8981e-4 \\ C_{24} &= 7.0819e-9 \\ C_{42} &= 2.6827e-8\end{aligned}$$

$C_{03} = -3.0217e-4$   
 $C_{06} = -2.5691e-8$   
 $C_{22} = -1.3951e-5$   
 $C_{40} = -1.1548e-5$   
 $C_{60} = -5.3341e-8$

$$\begin{aligned} C_{04} &= 4.2638e-6 \\ C_{20} &= -4.1060e-3 \\ C_{23} &= -4.2753e-7 \\ C_{41} &= 2.7378e-7 \end{aligned}$$
$$\begin{aligned}C_{02} &= -3.0337e-3 \\ C_{05} &= 4.8603e-7 \\ C_{21} &= -1.1772e-5 \\ C_{24} &= 3.7445e-8 \\ C_{42} &= 8.9223e-9\end{aligned}$$

$C_{03} = -4.9544e-4$   
 $C_{06} = -2.9443e-7$   
 $C_{22} = -1.2226e-5$   
 $C_{40} = 6.4273e-7$   
 $C_{60} = -1.2288e-8$

$$\begin{aligned} C_{04} &= 3.1402e-5 \\ C_{20} &= -2.5940e-3 \\ C_{23} &= -3.7638e-7 \\ C_{41} &= 2.1664e-7 \end{aligned}$$

# Numerical Embodiment 13

Read Width of Original: 222, Imaging Magnification: -0.1653,  
NA at Original Side: 0.0187,  $f_{eq} = -37.69$

i	Yi	Zi	$\theta_i$	Di	N <sub>di</sub>	Effective Size (X*Y)	
1	0.00	-220.44	0.0	220.14	1.		Object Surface (Original Surface)
2	0.00	0.00	0.0	4.80	1.	26.43*8.61	Transmitting Surface
3	0.00	4.80	45.0	9.10	1.	22.67*12.49	Reflecting Surface
4	-9.10	4.80	-45.0	4.60	1.	13.7*9.25	Reflecting Surface
5	-9.10	9.40	0.0	3.70	1.	8.52*6.4	Transmitting Surface (Stop)
6	-9.10	13.10	-45.0	8.80	1.	11.58*9.09	Reflecting Surface
7	-0.30	13.10	45.0	7.50	1.	17.93*8.46	Reflecting Surface
8	-0.30	20.60	45.0	4.50	1.	24.11*8.43	Reflecting Surface
9	-4.80	20.60	0.0	19.60	1.	26.06*4.76	Transmitting Surface
10	-24.40	20.60			1.		Image Plane (Sensor Surface)

## Aspherical Shape

### R3 Surface

$C_{02} = -5.4809e-3$	$C_{03} = 3.4337e-5$	$C_{04} = -3.6004e-6$
$C_{05} = 2.6877e-7$	$C_{06} = -2.4954e-8$	$C_{20} = -1.9618e-3$
$C_{21} = 5.1735e-5$	$C_{22} = 3.6712e-6$	$C_{23} = -1.6683e-8$
$C_{24} = -2.2272e-8$	$C_{40} = 1.9458e-6$	$C_{41} = -1.2257e-7$
$C_{42} = 9.7772e-9$	$C_{60} = -2.9597e-9$	

### R4 Surface

$C_{02} = -6.4075e-3$	$C_{03} = 5.6236e-5$	$C_{04} = -1.1591e-5$
$C_{05} = 1.1804e-6$	$C_{06} = -1.4678e-7$	$C_{20} = 1.5647e-3$
$C_{21} = 1.2100e-4$	$C_{22} = 1.0886e-5$	$C_{23} = -7.7632e-8$
$C_{24} = -7.7304e-8$	$C_{40} = -2.2614e-6$	$C_{41} = 5.2751e-7$
$C_{42} = 6.0420e-8$	$C_{60} = -1.8242e-8$	

### R6 Surface

$C_{02} = -2.5558e-3$	$C_{03} = -9.2337e-6$	$C_{04} = -1.0277e-5$
$C_{05} = 1.2682e-6$	$C_{06} = 3.1807e-7$	$C_{20} = -4.5515e-3$
$C_{21} = -1.1623e-4$	$C_{22} = 2.5157e-5$	$C_{23} = 1.4727e-6$
$C_{24} = -3.7813e-8$	$C_{40} = -6.2042e-6$	$C_{41} = 5.0551e-7$
$C_{42} = -2.1435e-7$	$C_{60} = -2.8678e-9$	

Approved for Release by NSA on 08-25-2014 pursuant to E.O. 13526



### R7 Surface

$C_{02}=-1.6417e-3$	$C_{03}=-1.6584e-4$	$C_{04}=-4.9779e-5$
$C_{05}=-6.6672e-7$	$C_{06}=3.5971e-7$	$C_{20}=5.8301e-4$
$C_{21}=-3.4856e-4$	$C_{22}=1.3360e-5$	$C_{23}=2.5606e-6$
$C_{24}=7.2100e-8$	$C_{40}=-3.4302e-6$	$C_{41}=8.9415e-7$
$C_{42}=-3.5448e-8$	$C_{60}=-9.6893e-9$	

## R8 Surface

$C_{02}=-6.2829e-3$	$C_{03}=-7.2993e-5$	$C_{04}=-3.6153e-5$
$C_{05}=-8.4251e-7$	$C_{06}=-1.1745e-7$	$C_{20}=-4.3172e-3$
$C_{21}=-2.2609e-4$	$C_{22}=-1.0428e-5$	$C_{23}=9.3647e-7$
$C_{24}=1.5891e-7$	$C_{40}=4.3128e-6$	$C_{41}=4.2867e-7$
$C_{42}=3.4859e-8$	$C_{60}=-3.8820e-9$	

# Numerical Embodiment 14

Read Width of Original: 222, Imaging Magnification: -0.1653,  
NA at Original Side: 0.0187,  $f_{eq}$ : -39.96

i	Yi	Zi	$\theta_i$	Di	N <sub>di</sub>	Effective Size (X*Y)	Object Surface
1	0.00	205.31	0.0	205.31	1.		(Original Surface)
2	0.00	0.00	0.0	4.50	1.	31.65*8.33	Transmitting Surface
3	0.00	4.50	45.0	8.80	1.	28.04*12.02	Reflecting Surface
4	-8.80	4.50	45.0	7.50	1.	18.81*8.41	Reflecting Surface
5	-8.80	-3.00	-45.0	3.60	1.	13.17*7.11	Reflecting Surface
6	-12.40	-3.00	0.0	3.60	1.	9.08*5.06	Transmitting Surface (Stop)
7	-16.00	-3.00	-45.0	7.20	1.	11.34*7.07	Reflecting Surface
8	-16.00	4.20	45.0	5.00	1.	16.11*9.31	Reflecting Surface
9	-21.00	4.20	0.0	19.93	1.	20.22*5.39	Transmitting Surface
10	-40.93	4.20			1.		Image Plane (Sensor Surface)

## Aspherical Shape

### R3 Surface

$C_{02}=-7.7942e-3$	$C_{03}=1.5340e-4$	$C_{04}=-7.6742e-6$
$C_{05}=3.2773e-7$	$C_{06}=1.0105e-8$	$C_{20}=-1.0191e-3$
$C_{21}=6.2260e-5$	$C_{22}=-9.2241e-7$	$C_{23}=-3.0462e-8$
$C_{24}=-8.8061e-10$	$C_{40}=2.0586e-6$	$C_{41}=-1.3894e-7$
$C_{42}=8.3907e-9$	$C_{60}=-2.4566e-9$	

### R4 Surface

$C_{02}=-7.2728e-3$	$C_{03}=-4.2030e-4$	$C_{04}=-2.0491e-5$
$C_{05}=-4.8447e-7$	$C_{06}=-9.7181e-8$	$C_{20}=-9.2280e-4$
$C_{21}=3.2208e-4$	$C_{22}=8.2382e-6$	$C_{23}=-2.5361e-6$
$C_{24}=-3.8347e-7$	$C_{40}=-6.7741e-6$	$C_{41}=-3.9460e-7$
$C_{42}=-8.1632e-8$	$C_{60}=-1.0713e-8$	

### R5 Surface

$C_{02}=3.1883e-3$	$C_{03}=-6.1203e-4$	$C_{04}=3.8105e-5$
$C_{05}=-2.7815e-6$	$C_{06}=-3.0068e-6$	$C_{20}=-6.3341e-3$
$C_{21}=4.8749e-4$	$C_{22}=2.9794e-5$	$C_{23}=1.0729e-6$
$C_{24}=-1.0564e-7$	$C_{40}=-6.1451e-6$	$C_{41}=9.1215e-7$
$C_{42}=7.5611e-8$	$C_{60}=2.1232e-8$	

## R7 Surface

$C_{02}=-8.5808e-3$	$C_{03}=-4.5399e-4$	$C_{04}=-1.1286e-5$
$C_{05}=-1.5372e-5$	$C_{06}=-1.5145e-6$	$C_{20}=6.6006e-3$
$C_{21}=2.2227e-4$	$C_{22}=3.3610e-5$	$C_{23}=2.7141e-6$
$C_{24}=-4.5924e-9$	$C_{40}=4.0853e-6$	$C_{41}=9.0088e-7$
$C_{42}=1.8614e-7$	$C_{60}=-6.3950e-8$	

### R8' Surface

$C_{02}=-1.3035e-2$	$C_{03}=-1.2855e-4$	$C_{04}=-7.7104e-6$
$C_{05}=-2.9888e-6$	$C_{06}=3.1345e-7$	$C_{20}=1.5832e-3$
$C_{21}=1.3213e-4$	$C_{22}=6.4279e-6$	$C_{23}=1.1227e-7$
$C_{24}=-5.6333e-8$	$C_{40}=1.1344e-5$	$C_{41}=1.1861e-6$
$C_{42}=1.0745e-7$	$C_{60}=-1.9480e-8$	

[illegible]

# Numerical Embodiment 15

Read Width of Original: 222, Imaging Magnification: -0.1653,  
NA at Original Side: 0.0187,  $f_{eq}$  : 37.55

i	Yi	Zi	$\theta_i$	Di	N <sub>di</sub>	Effective Size (X*Y)	
1	0.00	-210.46	0.0	210.46	1.		Object Surface (Original Surface)
2	0.00	0.00	0.0	5.00	1.	38.53*8.49	Transmitting Surface
3	0.00	5.00	45.0	9.50	1.	35.27*12.55	Reflecting Surface
4	-9.50	5.00	45.0	9.00	1.	24.18*10.4	Reflecting Surface
5	-9.50	-4.00	-45.0	5.00	1.	14.25*9.06	Reflecting Surface
6	-14.50	-4.00	0.0	4.50	1.	7.69*6.20	Transmitting Surface (Stop)
7	-19.00	-4.00	-45.0	8.50	1.	12.36*8.67	Reflecting Surface
8	-19.00	4.50	45.0	7.50	1.	21.0*9.22	Reflecting Surface
9	-26.50	4.50	45.0	6.00	1.	26.31*7.30	Reflecting Surface
10	-26.50	-1.50	0.0	14.54	1.	28.93*3.57	Transmitting Surface
11	-26.50	-16.04			1.		Image Plane (Sensor Surface)

## Aspherical Shape

### R3 Surface

$C_{02}=-3.9738e-3$	$C_{03}=1.6304e-4$	$C_{04}=-9.0512e-6$
$C_{05}=4.8201e-7$	$C_{06}=-9.1019e-9$	$C_{20}=-2.0427e-3$
$C_{21}=5.8600e-5$	$C_{22}=-1.3077e-6$	$C_{23}=-8.2015e-8$
$C_{24}=2.1265e-9$	$C_{40}=4.6160e-7$	$C_{41}=-5.6157e-8$
$C_{42}=3.0888e-9$	$C_{60}=-3.8991e-10$	

### R4 Surface

$C_{02}=-2.4559e-3$	$C_{03}=2.3458e-4$	$C_{04}=-4.8400e-6$
$C_{05}=-5.9899e-7$	$C_{06}=1.8301e-8$	$C_{20}=1.4498e-3$
$C_{21}=1.5853e-4$	$C_{22}=8.3292e-6$	$C_{23}=-6.0265e-7$
$C_{24}=-8.1035e-8$	$C_{40}=-1.3827e-6$	$C_{41}=-2.4613e-7$
$C_{42}=-2.2512e-8$	$C_{60}=1.7109e-9$	

### R5 Surface

$C_{02}=9.3479e-4$	$C_{03}=6.3740e-5$	$C_{04}=1.5280e-5$
$C_{05}=-1.0233e-6$	$C_{06}=-2.1499e-7$	$C_{20}=-2.4899e-3$
$C_{21}=7.1857e-5$	$C_{22}=2.5366e-5$	$C_{23}=8.7311e-7$
$C_{24}=-1.0984e-7$	$C_{40}=1.0442e-6$	$C_{41}=4.7624e-7$
$C_{42}=3.0322e-8$	$C_{60}=1.0869e-8$	

R7 Surface

$C_{02}=-1.3077e-3$	$C_{03}=-9.5358e-6$	$C_{04}=1.1644e-6$
$C_{05}=4.6743e-7$	$C_{06}=-2.1897e-7$	$C_{20}=-6.2673e-4$
$C_{21}=-9.9277e-5$	$C_{22}=1.1316e-5$	$C_{23}=9.8104e-8$
$C_{24}=-1.0288e-7$	$C_{40}=5.8473e-6$	$C_{41}=3.7217e-7$
$C_{42}=6.2029e-8$	$C_{60}=-1.1077e-8$	

R8 Surface

$C_{02}=-6.9421e-3$	$C_{03}=4.5103e-5$	$C_{04}=-8.8717e-6$
$C_{05}=5.3705e-7$	$C_{06}=-2.0675e-8$	$C_{20}=-5.6496e-3$
$C_{21}=-8.7333e-5$	$C_{22}=-8.6811e-7$	$C_{23}=-1.1882e-6$
$C_{24}=1.2747e-8$	$C_{40}=2.6056e-6$	$C_{41}=2.4906e-7$
$C_{42}=2.0119e-8$	$C_{60}=3.0389e-9$	

R9 Surface

$C_{02}=2.2767e-4$	$C_{03}=7.4454e-5$	$C_{04}=-5.2296e-6$
$C_{05}=-2.9920e-7$	$C_{06}=5.3685e-8$	$C_{20}=3.5672e-3$
$C_{21}=-2.9519e-5$	$C_{22}=-3.1213e-6$	$C_{23}=-1.0428e-6$
$C_{24}=1.3648e-7$	$C_{40}=-2.3563e-6$	$C_{41}=1.9318e-7$
$C_{42}=-1.6040e-8$	$C_{60}=5.8956e-10$	

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# Numerical Embodiment 16

Read Width of Original: 222, Imaging Magnification: -0.1653,  
NA at Original Side: 0.0187,  $f_{eq}$ : 43.13

i	Yi	Zi	$\theta_i$	Di	N <sub>di</sub>	Effective Size (X*Y)	
1	0.00	-239.61	0.0	239.61	1.		Object Surface (Original Surface)
2	0.00	0.00	0.0	5.00	1.	37.4*9.81	Transmitting Surface
3	0.00	5.00	45.0	10.30	1.	34.57*14.31	Reflecting Surface
4	-10.30	5.00	45.0	10.00	1.	23.88*10.99	Reflecting Surface
5	-10.30	-5.00	-45.0	5.50	1.	16.08*9.26	Reflecting Surface
6	-15.80	-5.00	0.0	6.00	1.	9.78*6.47	Transmitting Surface (Stop)
7	-21.80	-5.00	-45.0	9.00	1.	13.96*9.07	Reflecting Surface
8	-21.80	4.00	45.0	8.00	1.	20.74*8.98	Reflecting Surface
9	-29.80	4.00	-45.0	6.00	1.	24.27*6.20	Reflecting Surface
10	-29.80	10.00	0.0	10.39	1.	28.99*2.49	Transmitting Surface
11	-29.80	20.39			1.		Image Plane (Sensor Surface)

## Aspherical Shape

### R3 Surface

$C_{02}=-4.8976e-3$	$C_{03}=1.5273e-4$	$C_{04}=-1.0530e-5$
$C_{05}=3.6681e-7$	$C_{06}=-2.8231e-9$	$C_{20}=-1.9499e-3$
$C_{21}=5.0580e-5$	$C_{22}=-8.2125e-7$	$C_{23}=3.0451e-8$
$C_{24}=-4.1110e-10$	$C_{40}=8.7459e-7$	$C_{41}=-1.7593e-8$
$C_{42}=-3.2845e-10$	$C_{60}=8.5468e-11$	

### R4 Surface

$C_{02}=-3.7198e-3$	$C_{03}=2.0137e-4$	$C_{04}=-1.3162e-5$
$C_{05}=-1.5142e-6$	$C_{06}=2.9707e-8$	$C_{20}=3.2871e-4$
$C_{21}=2.1569e-4$	$C_{22}=3.8014e-6$	$C_{23}=2.2547e-7$
$C_{24}=4.1087e-8$	$C_{40}=-3.4195e-6$	$C_{41}=8.5940e-9$
$C_{42}=2.1575e-9$	$C_{60}=-2.6763e-9$	

### R5 Surface

$C_{02}=8.9718e-4$	$C_{03}=5.5441e-5$	$C_{04}=1.7587e-5$
$C_{05}=-8.9855e-7$	$C_{06}=-1.0873e-7$	$C_{20}=-4.5083e-3$
$C_{21}=1.9520e-4$	$C_{22}=1.6063e-5$	$C_{23}=1.3767e-6$
$C_{24}=7.1130e-8$	$C_{40}=-5.0059e-6$	$C_{41}=-1.1423e-7$
$C_{42}=-1.4689e-8$	$C_{60}=2.2482e-9$	

R7 Surface

$C_{02}=-7.3920e-4$	$C_{03}=2.8734e-5$	$C_{04}=3.9706e-6$
$C_{05}=5.2045e-7$	$C_{06}=-6.1714e-8$	$C_{20}=1.4253e-3$
$C_{21}=-1.0230e-4$	$C_{22}=1.0728e-6$	$C_{23}=9.0333e-7$
$C_{24}=-1.0870e-7$	$C_{40}=-4.7496e-6$	$C_{41}=-3.4478e-7$
$C_{42}=1.4200e-8$	$C_{60}=-2.8621e-9$	

R8 Surface

$C_{02}=-7.1121e-3$	$C_{03}=3.1998e-5$	$C_{04}=-1.0329e-5$
$C_{05}=-6.1094e-7$	$C_{06}=1.4211e-7$	$C_{20}=-5.8559e-3$
$C_{21}=-1.4938e-4$	$C_{22}=-9.6136e-6$	$C_{23}=5.3107e-7$
$C_{24}=-2.5542e-7$	$C_{40}=-1.7990e-6$	$C_{41}=1.3608e-7$
$C_{42}=2.5650e-8$	$C_{60}=1.0580e-8$	

R9 Surface

$C_{02}=-7.3487e-4$	$C_{03}=2.4984e-6$	$C_{04}=-9.0385e-6$
$C_{05}=-2.8895e-6$	$C_{06}=7.8261e-7$	$C_{20}=-3.0120e-3$
$C_{21}=-6.6311e-5$	$C_{22}=-1.6804e-5$	$C_{23}=1.5172e-6$
$C_{24}=-4.4455e-7$	$C_{40}=-5.2507e-6$	$C_{41}=2.1385e-8$
$C_{42}=9.5273e-9$	$C_{60}=1.7378e-8$	

# Numerical Embodiment 17

Read Width of Original: 305, Imaging Magnification: -0.22028,  
NA at Original Side: 0.0201,  $f_{eq}$ : 49.00

i	Yi	Zi	$\theta_i$	Di	N <sub>di</sub>	Effective Size (X*Y)	
1	0.00	-199.00	0.0	4.00	1.5		Object Surface (Original Surface)
2	0.00	-195.00	0.0	195.00	1.0		Transmitting Surface
3	0.00	0.00	0.0	10.00	1.0		Transmitting Surface
4	0.00	10.00	45.0	10.00	1.0	55.9*19.8	Reflecting Surface
5	-10.00	10.00	-45.0	12.00	1.0	30.7*12.7	Reflecting Surface
6	-10.00	-2.00	-45.0	-6.00	1.0	19.2*11.3	Reflecting Surface
7	-16.00	-2.00	0.0	-5.00	1.0		Transmitting Surface (Stop)
8	-21.00	-2.00	-45.0	10.00	1.0	15.1*8.8	Reflecting Surface
9	-21.00	-12.00	-45.0	-11.50	1.0	36.2*11.5	Reflecting Surface
10	-32.50	-12.00	45.0	10.00	1.0	49.1*10.5	Reflecting Surface
11	-32.50	-2.00	0.0	0.70	1.5		Transmitting Surface
12	-32.50	-1.30	0.0	19.70	1.0		Transmitting Surface
13	-32.50	18.40			1.0		Image Plane (Sensor Surface)

## Aspherical Shape

### R4 Surface

$C_02=-4.6370e-3$	$C_03=4.7956e-5$	$C_04=-3.8778e-7$
$C_05=-2.6373e-8$	$C_06=-4.1368e-10$	$C_20=-2.2522e-3$
$C_21=4.6045e-5$	$C_22=-6.4075e-7$	$C_23=-3.6626e-9$
$C_24=9.5021e-10$	$C_40=8.0691e-8$	$C_41=-1.2313e-9$
$C_42=-1.0275e-10$	$C_60=-4.4066e-12$	

### R5 Surface

$C_02=-7.9557e-3$	$C_03=-1.9354e-5$	$C_04=-1.7661e-7$
$C_05=-2.7155e-7$	$C_06=-1.7098e-8$	$C_20=-2.9139e-3$
$C_21=2.2513e-4$	$C_22=1.1500e-6$	$C_23=1.9226e-7$
$C_24=1.0393e-8$	$C_40=-3.1571e-6$	$C_41=2.1718e-10$
$C_42=-3.2272e-9$	$C_60=-2.2044e-10$	

### R6 Surface

$C_02=-7.3984e-3$	$C_03=-8.9040e-5$	$C_04=-3.3142e-6$
$C_05=-1.1728e-7$	$C_06=-1.2995e-8$	$C_20=-1.0503e-2$
$C_21=4.4162e-5$	$C_22=-5.6571e-7$	$C_23=2.8155e-7$
$C_24=6.6068e-9$	$C_40=-1.7855e-6$	$C_41=-1.8879e-8$
$C_42=-3.4977e-10$	$C_60=-3.6874e-10$	

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$C_{02} = -1.2363e-2$   
 $C_{05} = -3.5502e-7$   
 $C_{21} = 6.9852e-5$   
 $C_{24} = 6.2157e-8$   
 $C_{42} = -2.3096e-8$

$C_{03} = -2.3209e-4$   
 $C_{06} = -1.5995e-7$   
 $C_{22} = -1.4608e-5$   
 $C_{40} = 2.0029e-6$   
 $C_{60} = -1.3092e-8$

$$\begin{aligned}C_{04} &= -2.2229e-5 \\ C_{20} &= -1.2225e-2 \\ C_{23} &= 1.2372e-6 \\ C_{41} &= 3.8246e-7\end{aligned}$$

$C_{02} = -7.9876e-3$   
 $C_{05} = 1.5135e-7$   
 $C_{21} = 1.1755e-4$   
 $C_{24} = -1.0577e-9$   
 $C_{42} = -1.6593e-9$

$C_{03}=2.8932e-5$   
 $C_{06}=-2.6037e-9$   
 $C_{22}=-1.7268e-6$   
 $C_{40}=8.1403e-7$   
 $C_{60}=-1.0464e-11$

$$\begin{aligned}C_{04} &= -2.1422e-6 \\ C_{20} &= -6.9135e-3 \\ C_{23} &= 2.3870e-7 \\ C_{41} &= 2.7851e-8\end{aligned}$$

$C_{02}=8.2240e-4$   
 $C_{05}=2.9663e-7$   
 $C_{21}=4.4682e-5$   
 $C_{24}=1.4368e-9$   
 $C_{42}=1.2792e-19$

$C_{03}=1.3187e-4$   
 $C_{06}=-4.2567e-9$   
 $C_{22}=3.6473e-6$   
 $C_{40}=-7.9626e-7$   
 $C_{60}=2.5752e-19$

$$\begin{aligned}C_{04} &= -6.7315e-6 \\ C_{20} &= 4.3524e-3 \\ C_{23} &= 5.7219e-8 \\ C_{41} &= -1.5383e-8\end{aligned}$$

According to the present invention, in an original reading system such as a digital copier of which a high speed and high resolution are required, there can be achieved an original reading imaging  
5 optical system which can easily realize an integral carriage type scanning process, and an image reading apparatus using the same.

Besides, according to the present invention, in the reading of a digital color image, there can be  
10 achieved an original reading imaging optical system which is free of chromatic aberration and can easily realize an integral carriage type scanning process, and an image reading apparatus using the same.

Besides, according to the present invention,  
15 there can be achieved an original reading imaging optical system which, even if an imaging optical system is comprised of off-axial reflecting surfaces, suffers little from the occurrence of an asymmetrical aberration and is not greatly deteriorated in optical  
20 performance, and an image reading apparatus using the same.